

# Status and perspective of the Nb<sub>3</sub>Al development in Japan

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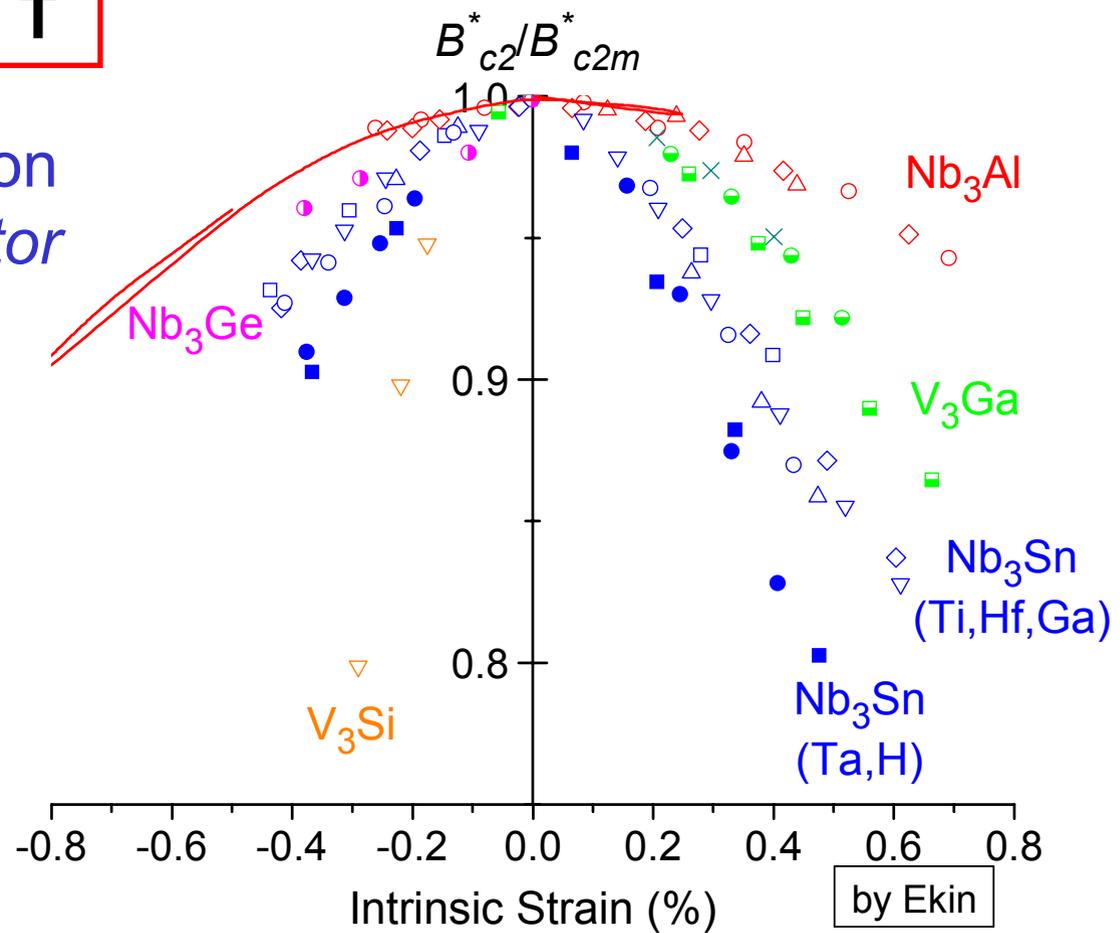
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*High Energy Accel. Res. Organ. (KEK)*

# Advantages of RHQT Nb<sub>3</sub>Al over Nb<sub>3</sub>Sn

**better strain tolerance**  
**higher  $B_{c2}(4.2K)$ : 30 T**

Large scale application  
*Fusion, Accelerator*



# Advantages of RHQT Nb<sub>3</sub>Al over HTS

- Easy superconducting joint
- Large  $n$ -value
- Tolerance to stress and strain

## *Application*



- High-field NMR spectroscopy

# Specification of Nb<sub>3</sub>Al conductor for NMR uses

- Rectangular
- Stabilizer (Cu clad)
- Nb matrix (superconducting)
- DC (filament diameter, spacing)
- Optimization of J<sub>c</sub> (4.2K) at 21 T

# Advanced A15 Compounds

- $Nb_3Al$
- $Nb_3Ga$
- $Nb_3(Al,Ge)$

Off-stoichiometry at LT



New approach

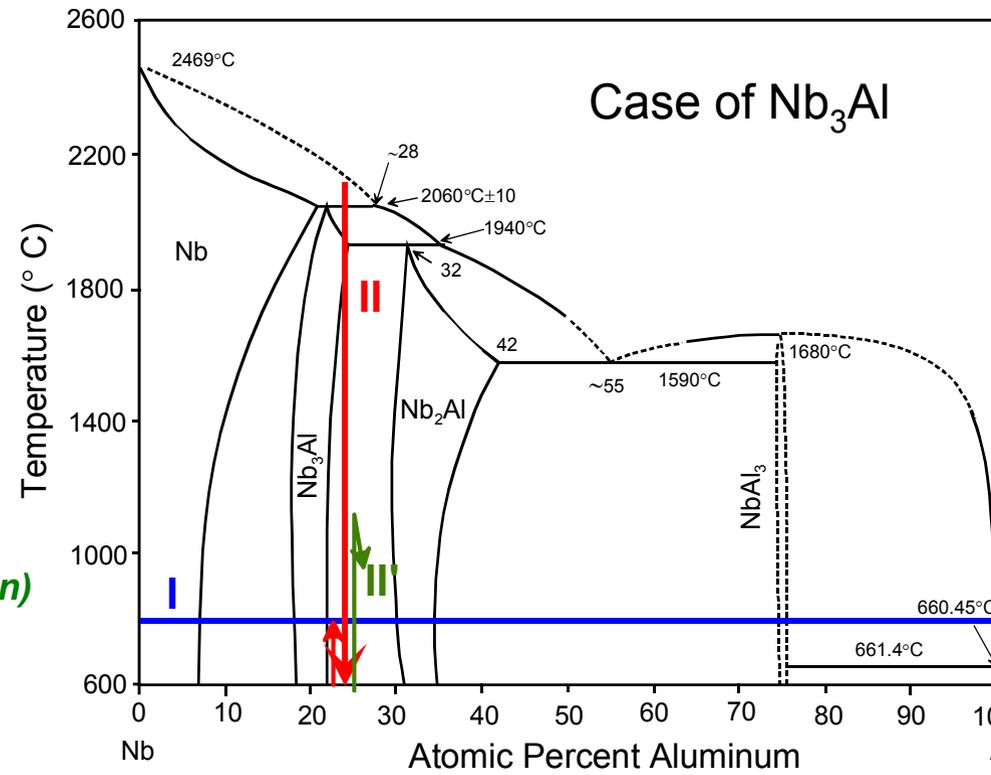
**RHQT technique**

(rapid-heating, quenching and transformation)

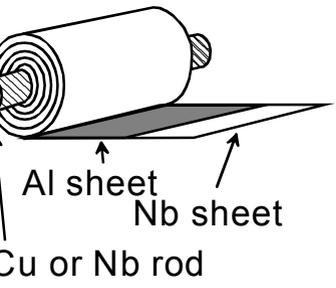
stoichiometry

without grain growth

without grain coarsening



Manufacture: binary reaction, Al dimension: < 100nm

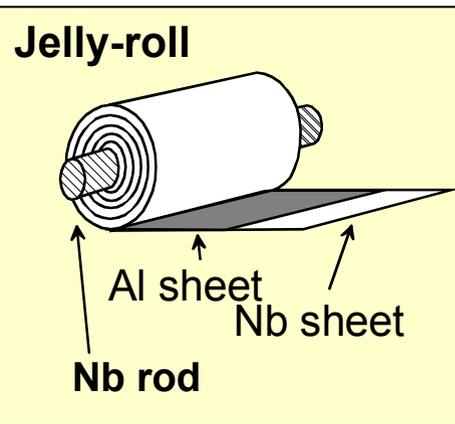


Diffusion process (750 $^{\circ}C$  x 50h)  
 11-14 T, off-stoichiometry  
 Cu-matrix JR

**RHQT process (1900 $^{\circ}C$  + 800 $^{\circ}C$ x10h)**  
 12-23 T, stacking faults  
 Nb-matrix JR

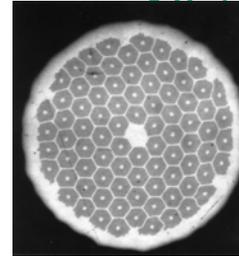
New process (TRUQ, DRHQ)  
 21-25 T

# Rapid Heating, Quenching and Transformation process



*Extrusion + Drawing*

Precursor : Nb/JR



*Joule Heating + Quenching*

Nb/Nb(Al)<sub>ss</sub>

bcc supersaturated solid solution

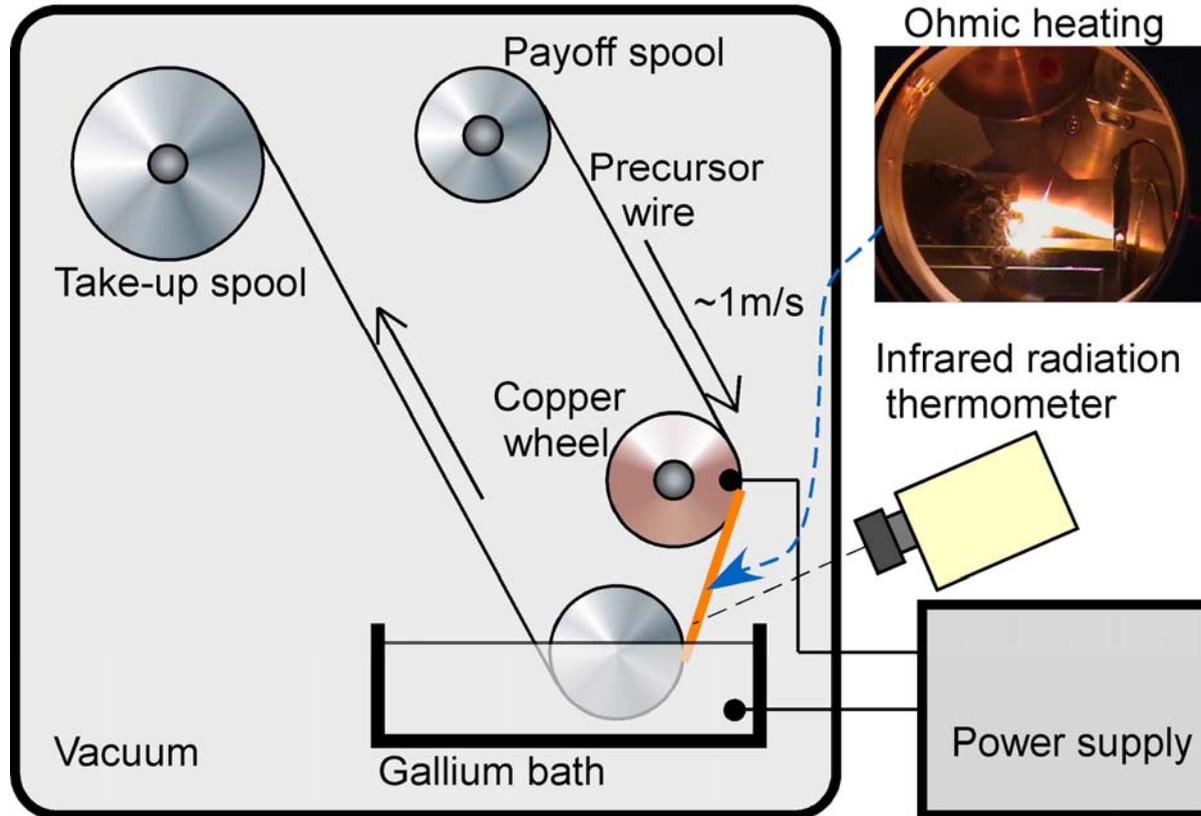
*Cu cladding*

Cu/Nb/Nb(Al)<sub>ss</sub>

*Winding + Transformation*

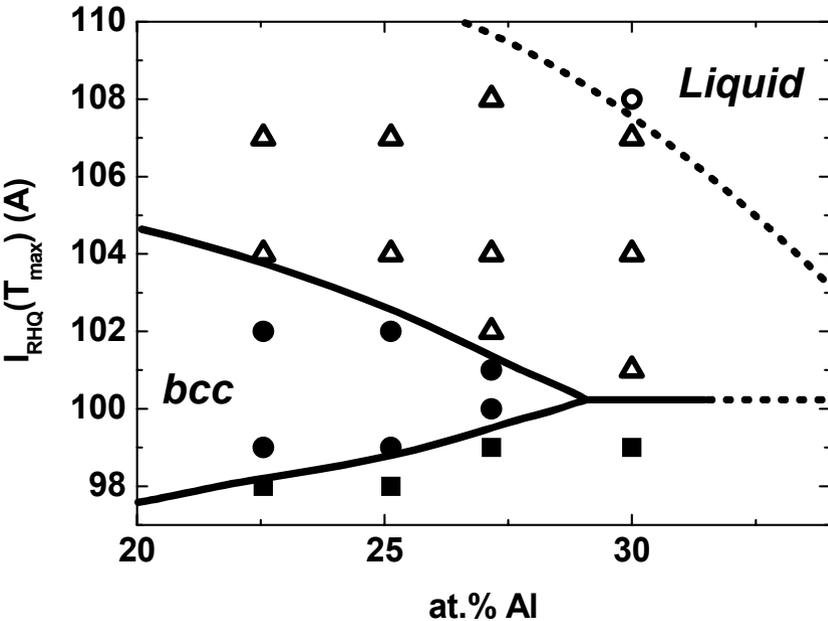
Cu/Nb/Nb<sub>3</sub>Al

stoichiometry fine grain

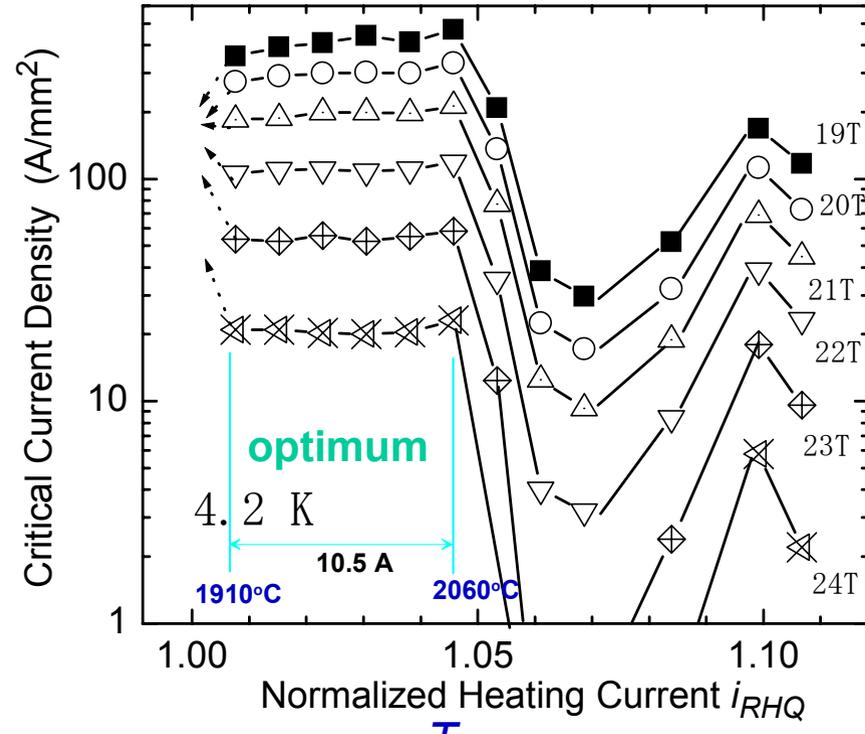
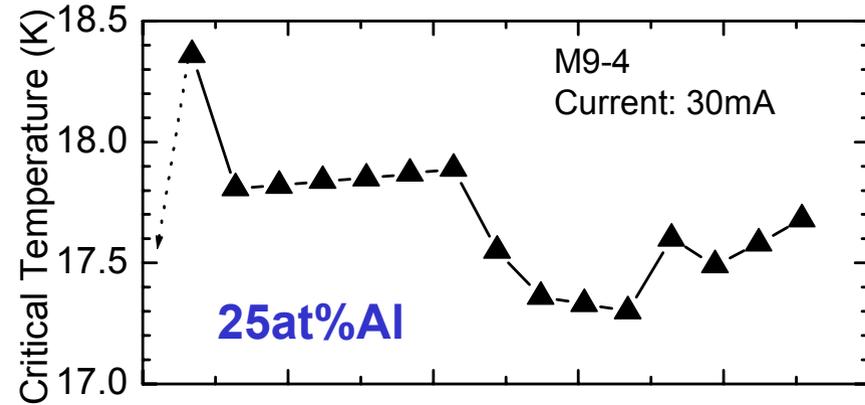


# Long-length of RHQ processing

- Plateau region (150°C): optimum
- Insensitivity to unwanted temperature scatter
- Uniformity of SC properties along a long-length of wire

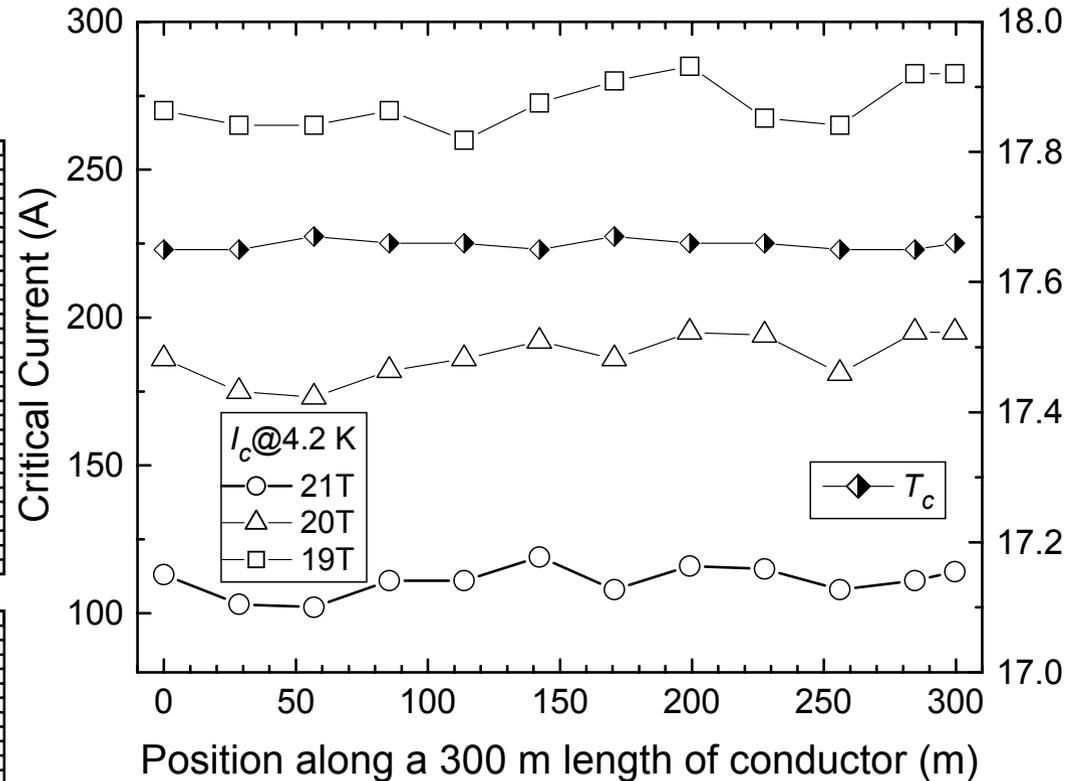
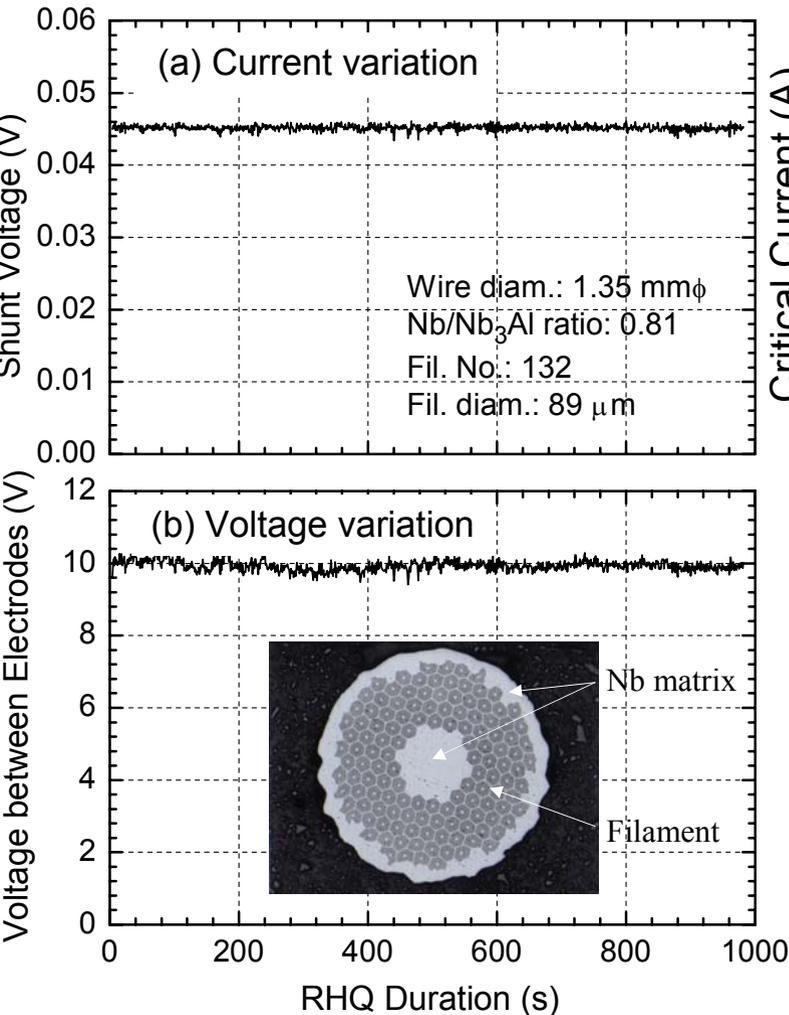


	solid solution	melting	melting
A15+ $\sigma$ brittle	bcc ductile	Al-poor bcc + liquid (not brittle)	bcc ductile



# Distributions of $T_c$ and $J_c$ along a 300 m length of wire

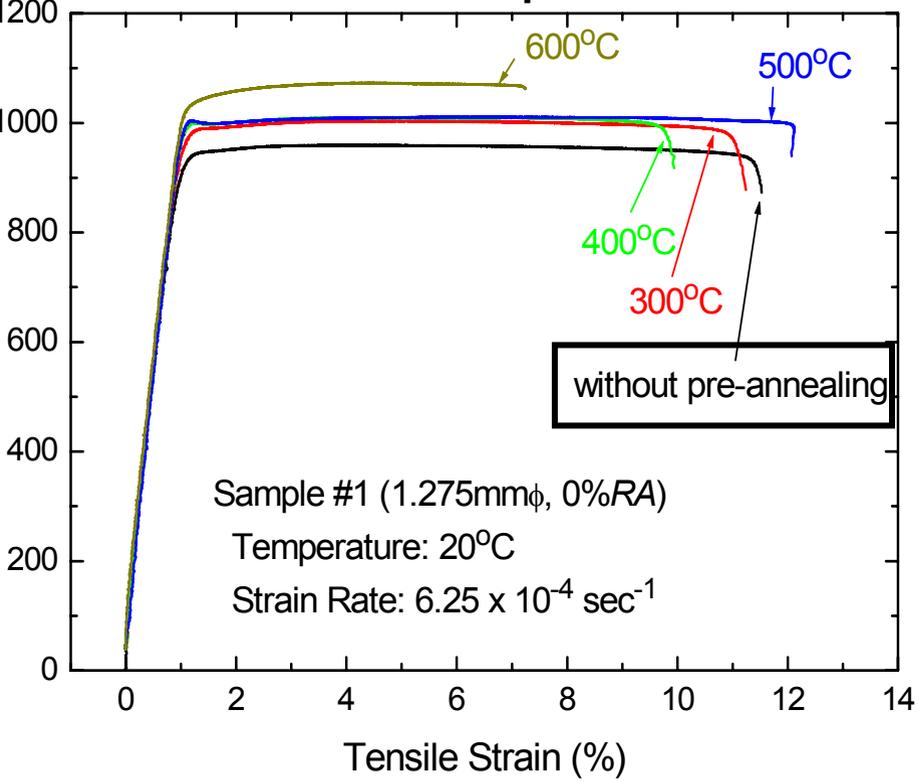
Constant current power supply



Standard deviation of  $J_c$  (4.2K&21T) : 5 %

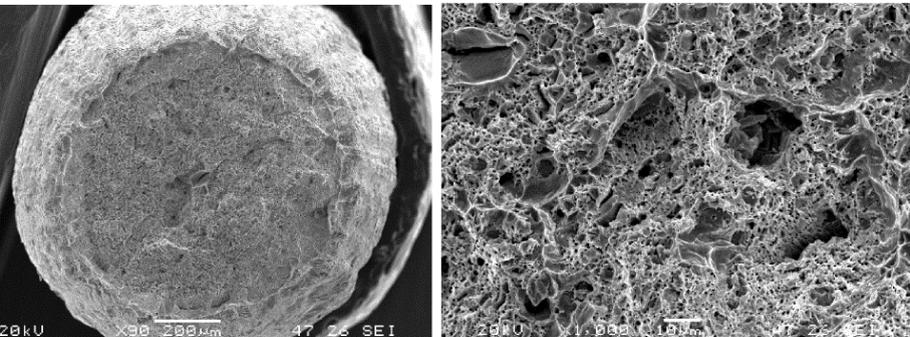
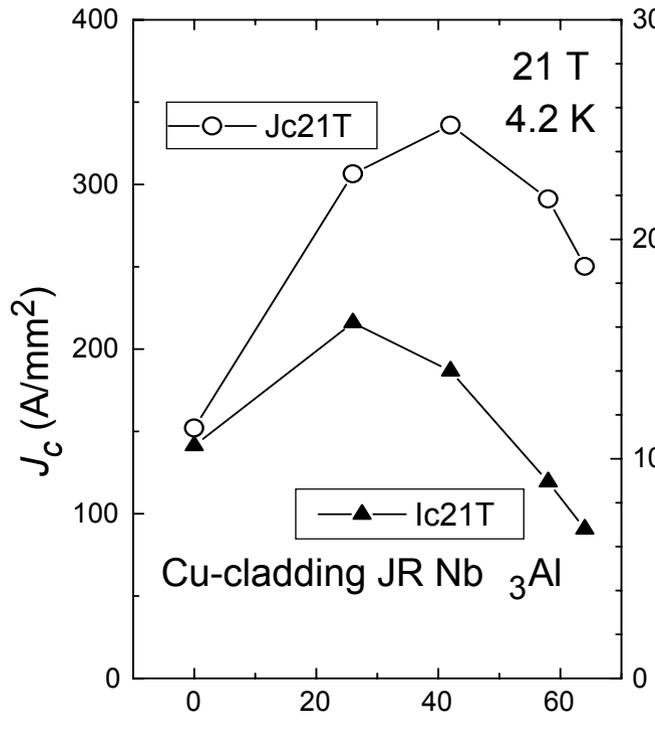
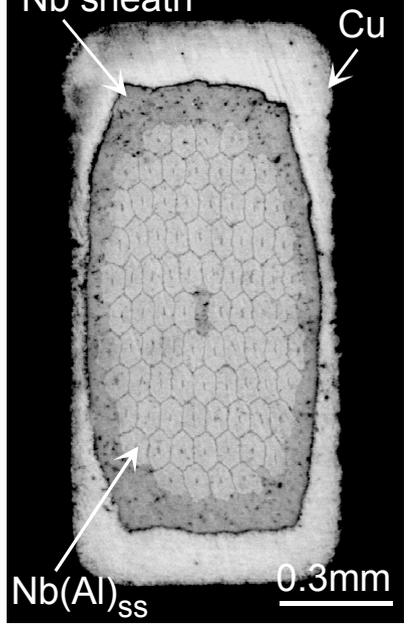
# Deformability of Nb(Al)<sub>ss</sub> at RT

Tensile test at room temperature

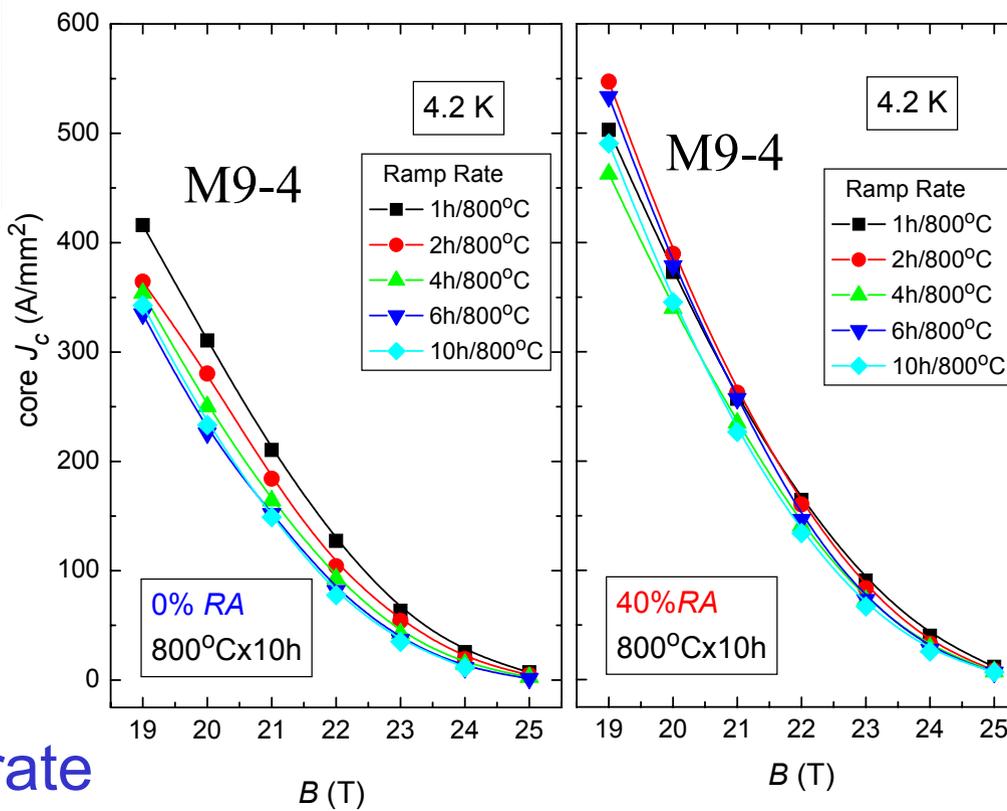
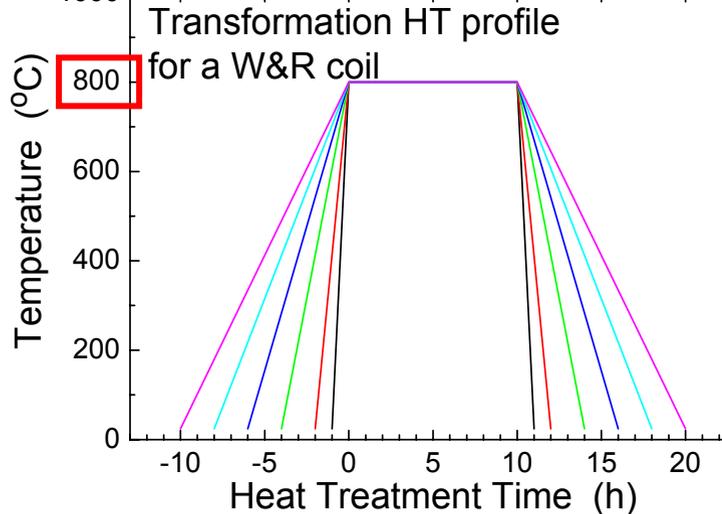
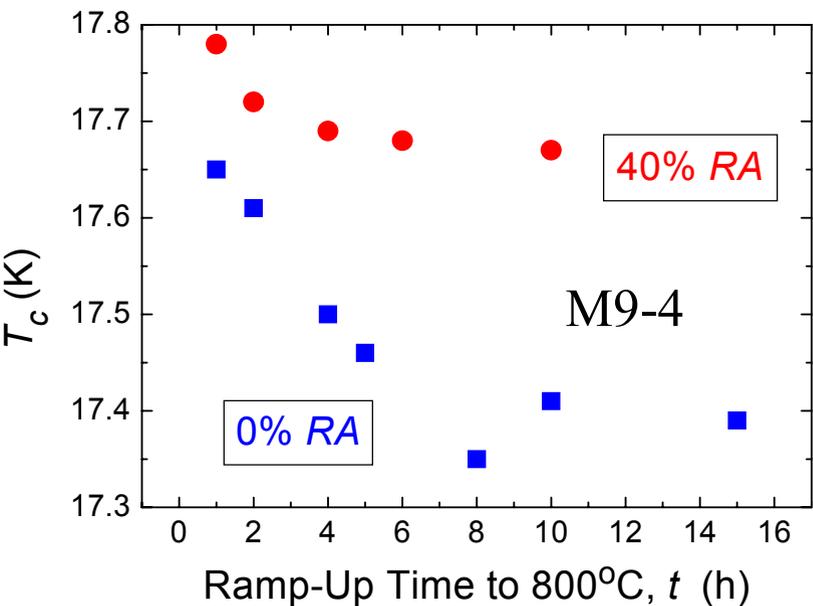


Incorporation of Cu stabilizer by mechanical cladding

J<sub>c</sub> improvement



# Temperature ramp-up rate at transformation annealing



Deformation

$J_c$  enhancement  
Less sensitive to ramp rate

# Coil specifications

TABLE I

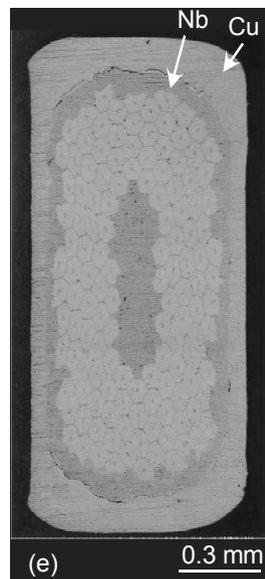
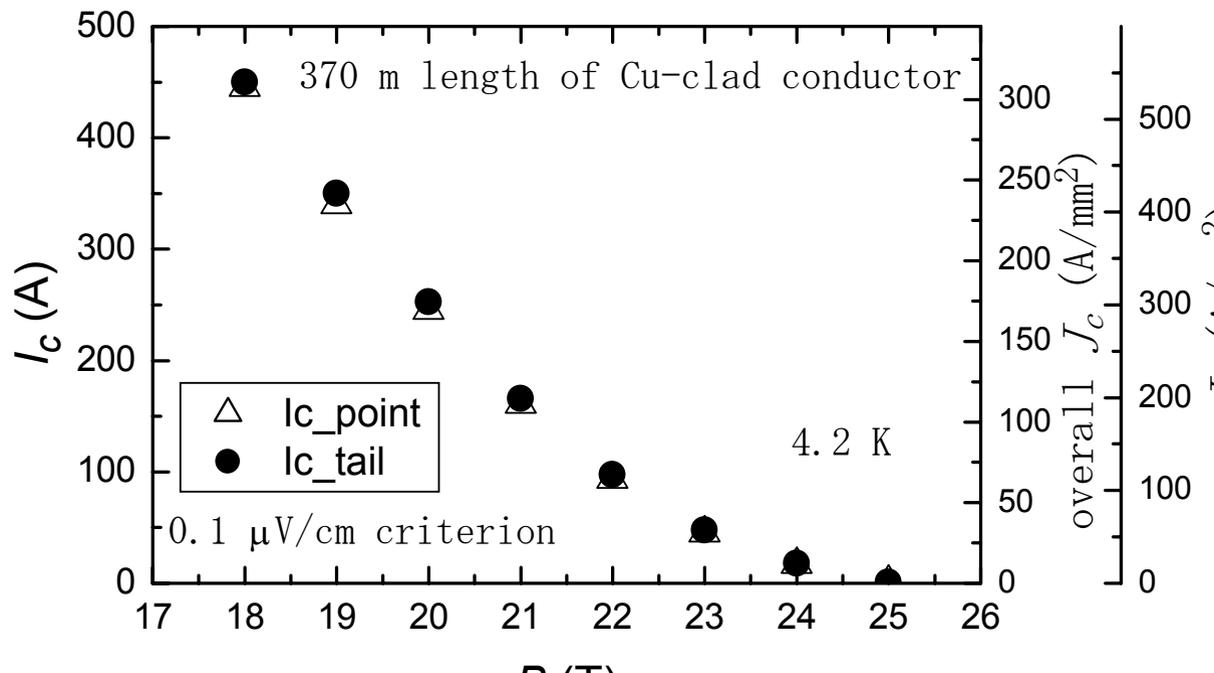
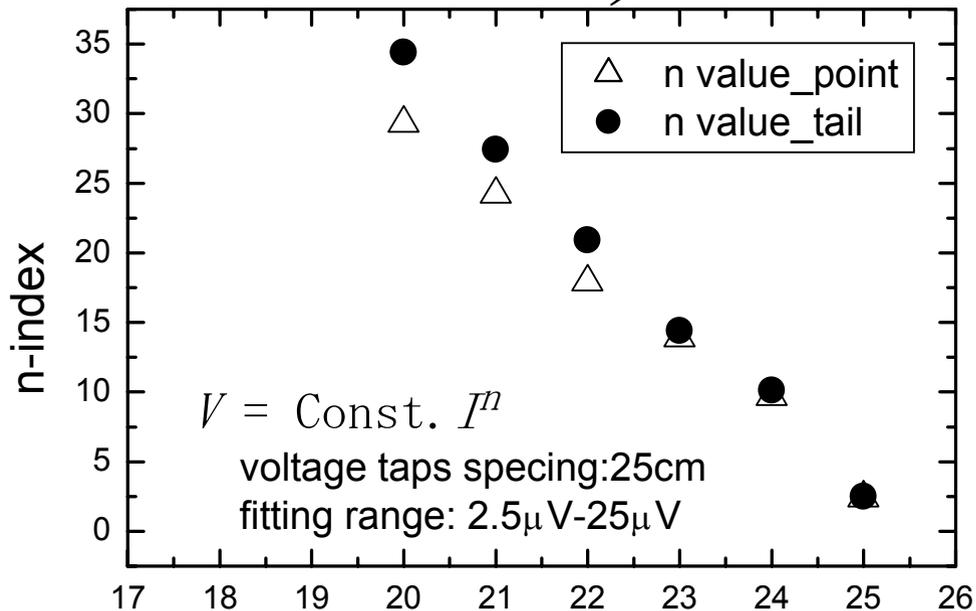
SPECIFICATIONS OF WIND & REACT  $Nb_3Al$  SOLENOID COILS

	Previous M11-1	Present ME332	Present ME356
HQT JR $Nb_3Al$ conductor			
Stabilizer	Cu-clad	Cu-clad	Cu-clad
Piece length (m)	35	370	370
Cross section ( $mm^2$ )	1.61x0.71	1.82x0.84	1.81x0.80
Filament diameter	70	74	75.5
Number of filaments	84	132	132
Cu/non-Cu ratio	0.45	0.38	0.39
Insulator	$Al_2O_3$ fiber	$Al_2O_3$ fiber	$Al_2O_3$ fiber
Winding			
Inner diameter (mm)	19.7	90.2	64.6
Outer diameter (mm)	40.8	111.8	99.3
Height (mm)	49.7	200	132.4
Number of turns	311	949	988
Total length of wire	30	300.5	254
Soil			
Impregnation	Beeswax	Beeswax	Beeswax
Transformation	<u>RT</u> →(5h)→800°C→(10h)→800°C→RT		
Coil constant (T/A)	0.00106	0.00562	0.00797

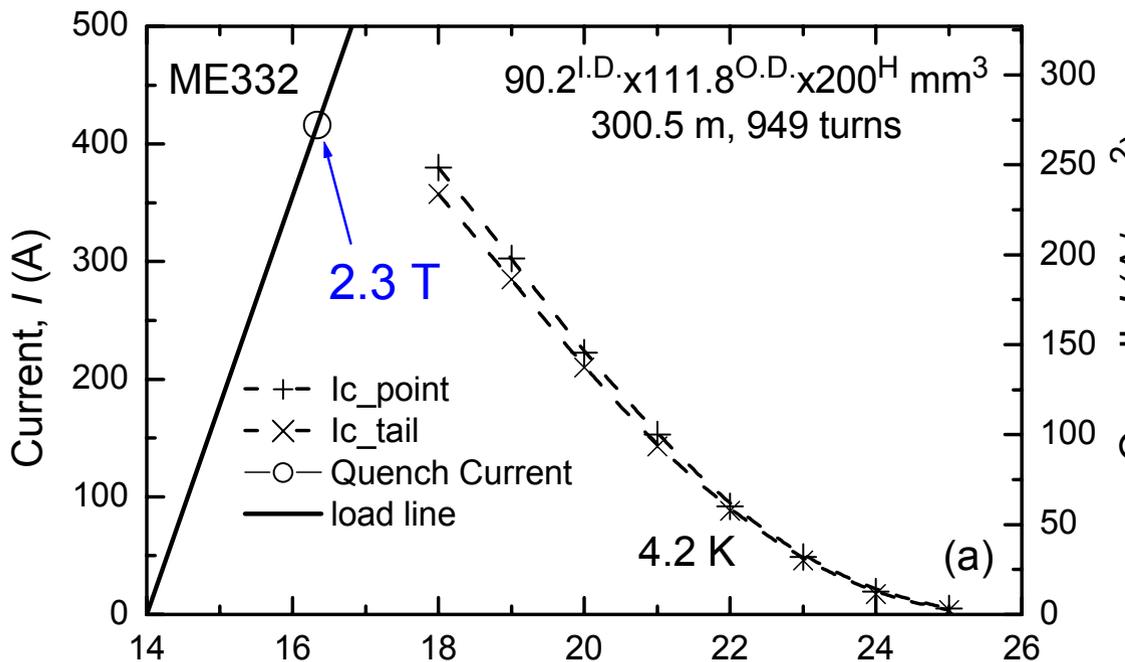


$n$ -value ( $10^{-5} - 10^{-4}$  V/m)

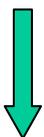
Consistency of  $I_c$   
point, tail of 370 m  
 $n$ -value  
**25@21T,4.2K**



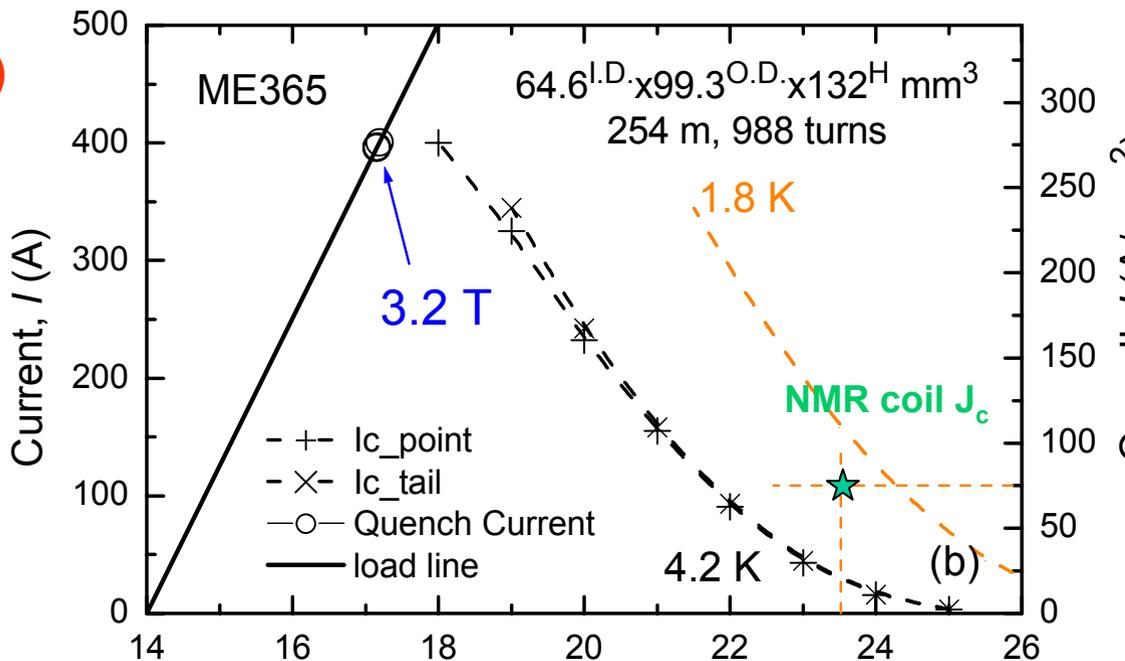
# • Loading test



$I_q$  (coil) > 0.9  $I_c$  (short samples)

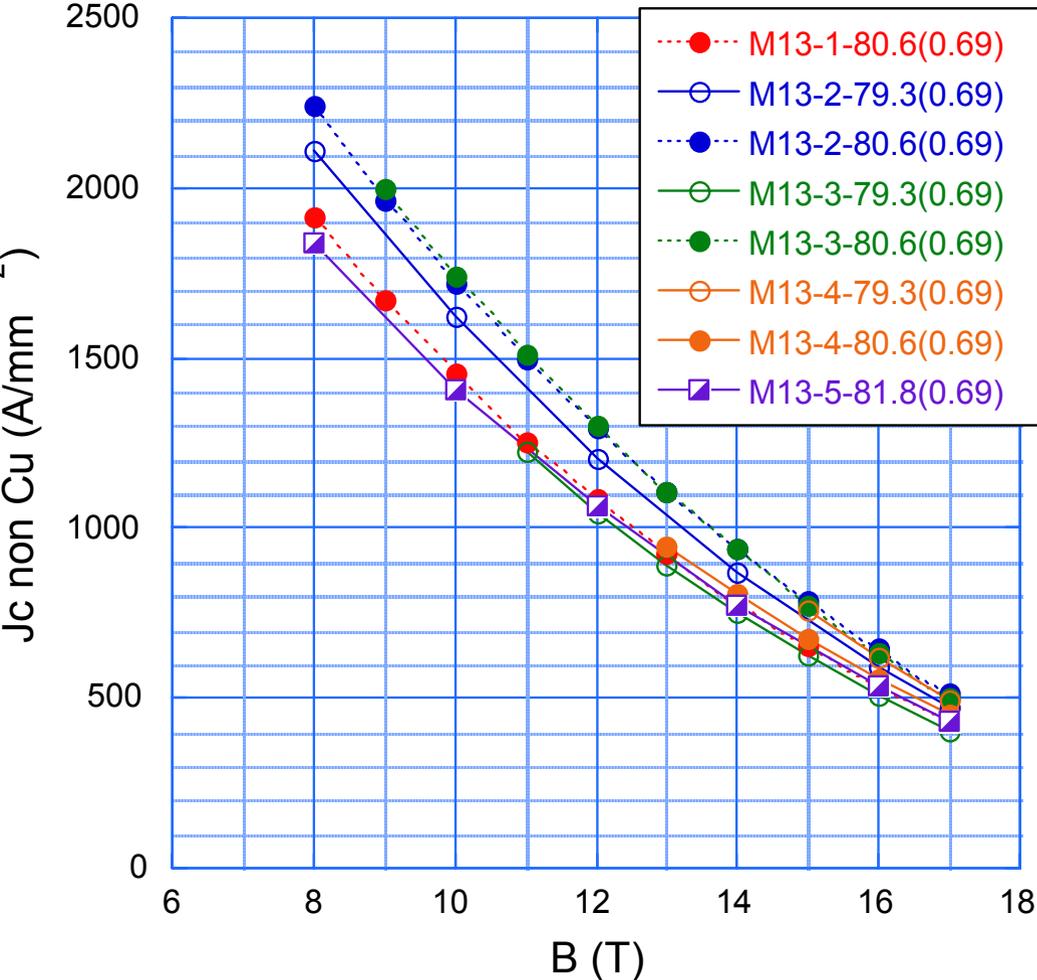
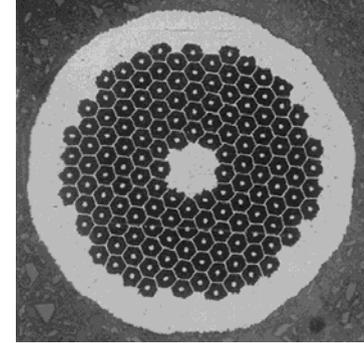


Uniformity of a long-length  
 of RHQ operation over 300 m

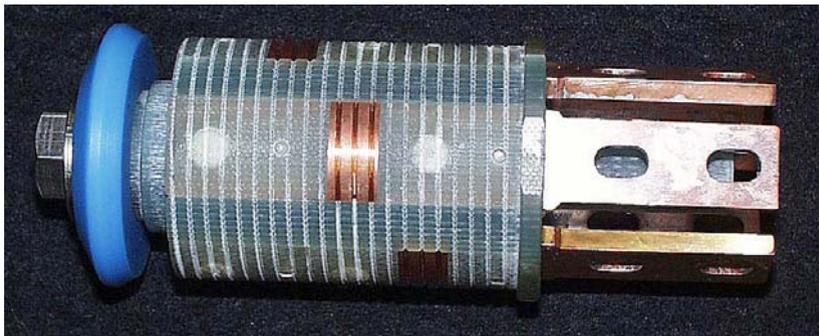


• RHQT  $\text{Nb}_3\text{Al}$  is really reliable  
 for practical coil application.

# KEK



- 1 kA  $I_c$  probe
- Measurement of  $J_c$  of round wire electroplated with Cu in fields from 8 to 17 T
- Optimization  
wire diameter: 0.8  $\rightarrow$  0.69 mm  
RA: 20% (< 40% for 21T)  
transformation HT: 775°C15h
- Highest  $J_c$ : 1730 A/mm<sup>2</sup> at 10 T



**Sample length:** 300 mm  
**Large cross section of Cu:** 72 mm<sup>2</sup>  
**Heating at 1000 A:** < 80 mW/lead  
( $\Delta T < 10$  mK)

# Internal Stabilization

Less expensive

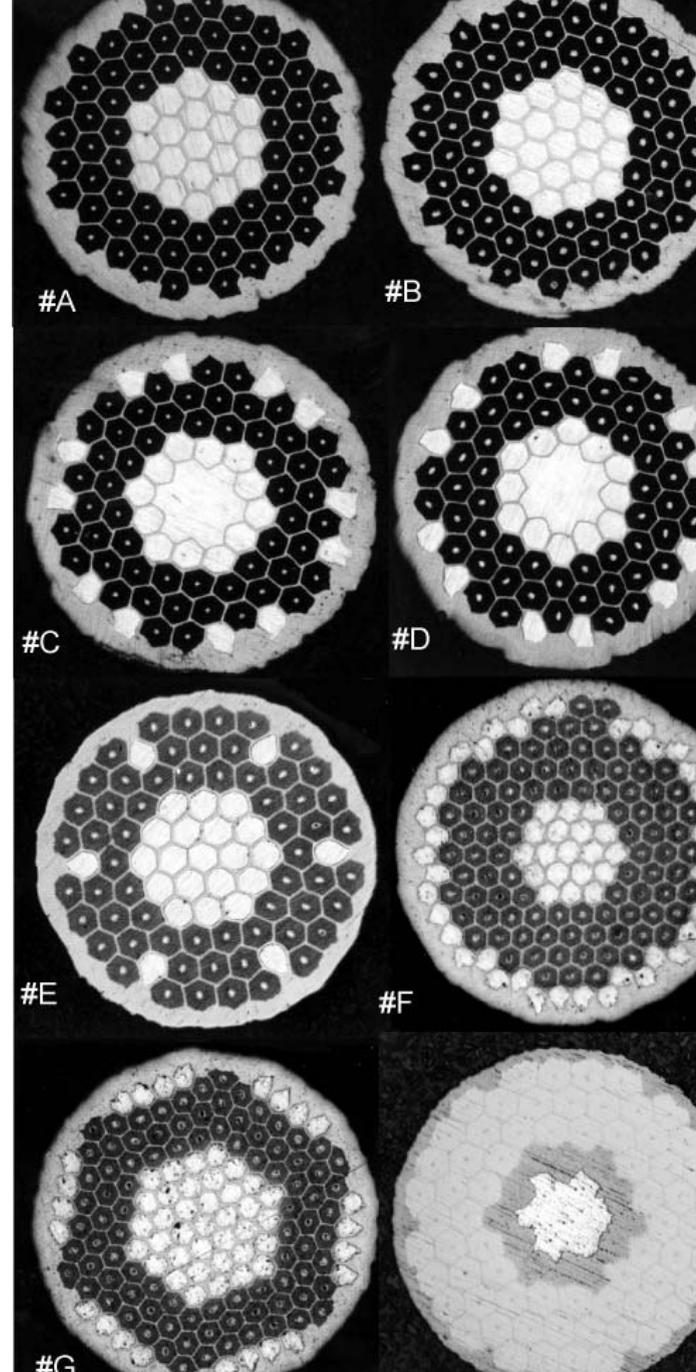
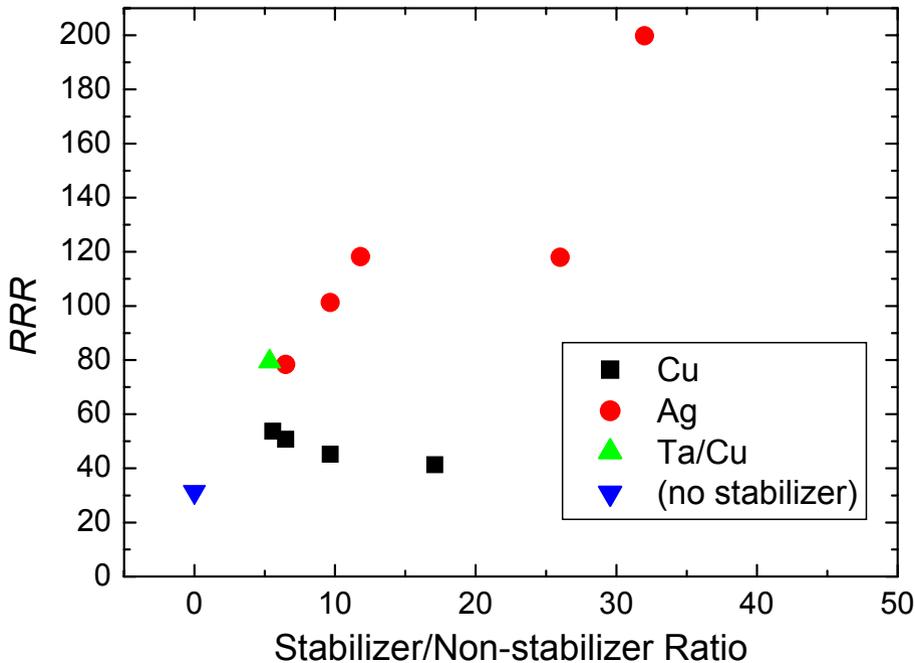
Round cross section of wire

Possible high current conductors (CICC, Rutherford cables, etc)

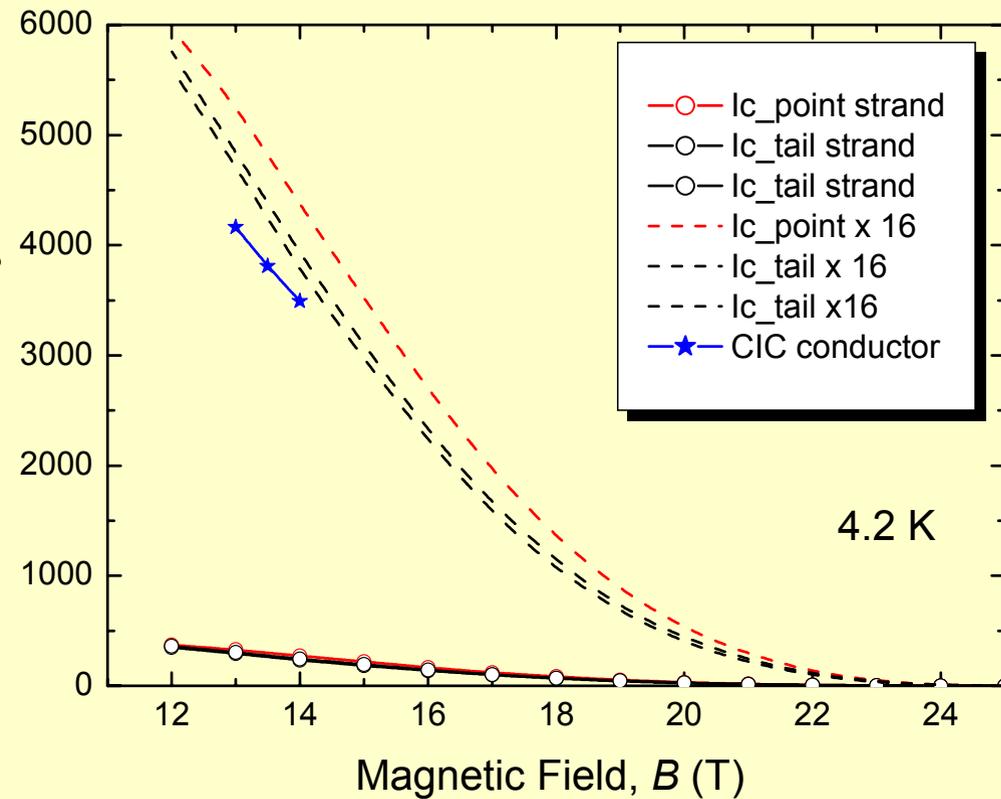
No contamination of Ag with Ga

Large RRR (200)

Applicability to high temperature transformation (TRUQ, DRHQ)



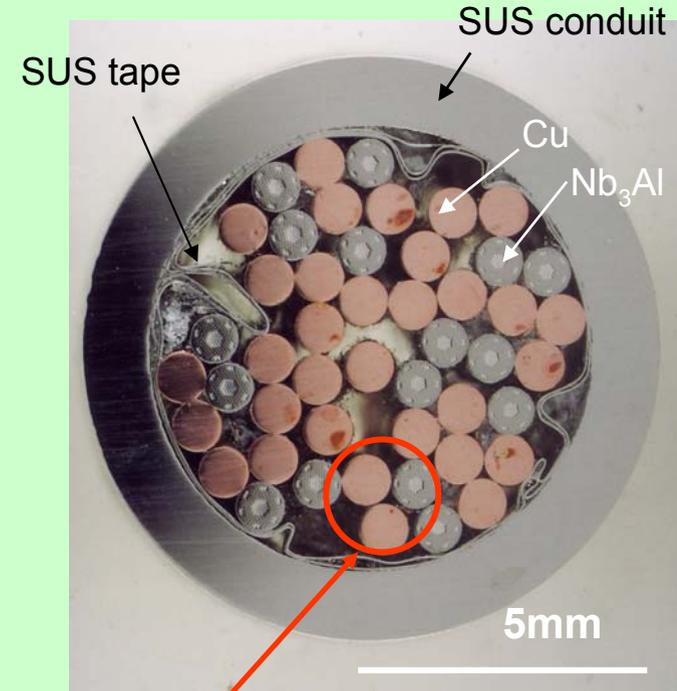
# Trial Manufacture of High-Current RHQT Nb<sub>3</sub>Al Conductors



$I_c$  at 14 T  
 Measure: 3.49 kA  
 Design ( $I_{c, \text{strand}} \times 16$ ): 3.7 – 4.3 kA

7% degradation

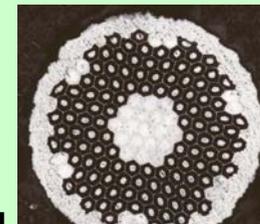
## Cable-in-Conduit Conductor for Fusion Uses



The 1<sup>st</sup> triplet: a Nb<sub>3</sub>Al, two Cu

The third stage cable: 3 x 4 x 4

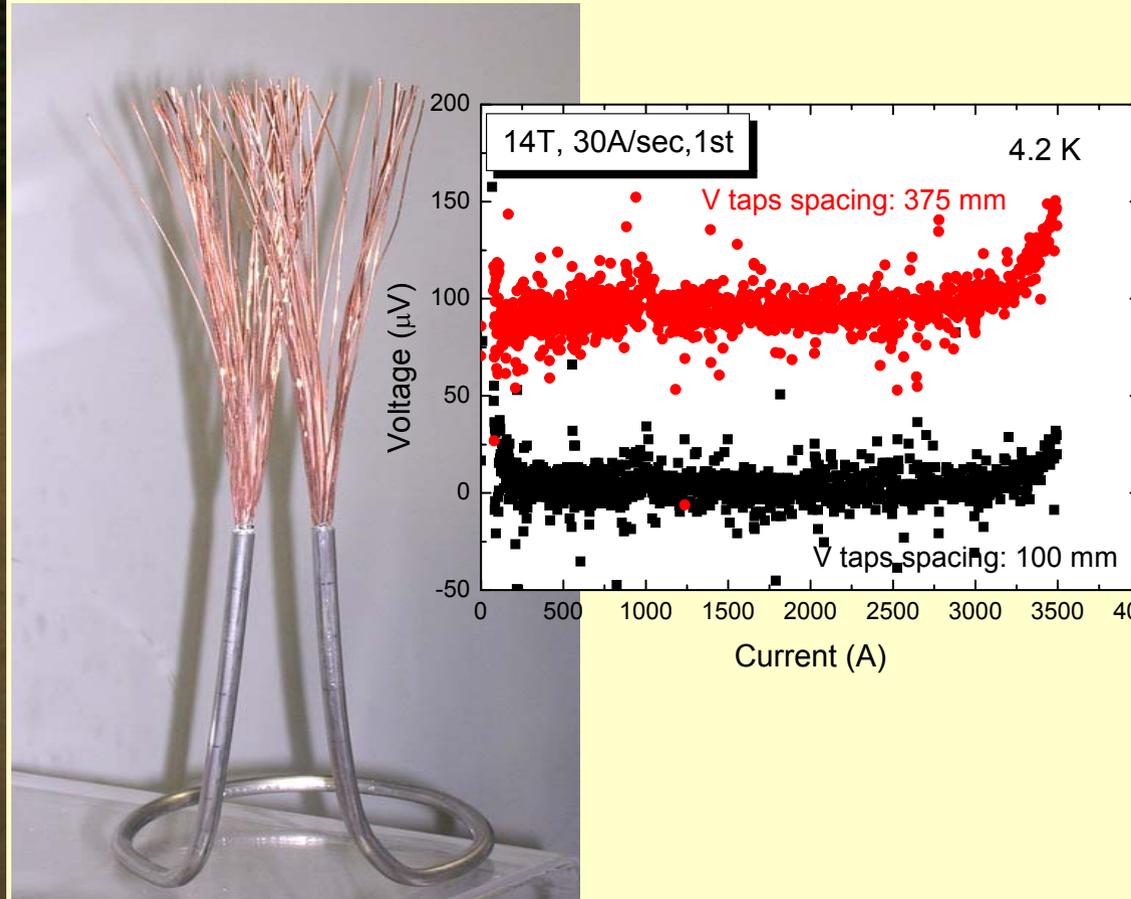
Internally stabilized Nb<sub>3</sub>Al strand

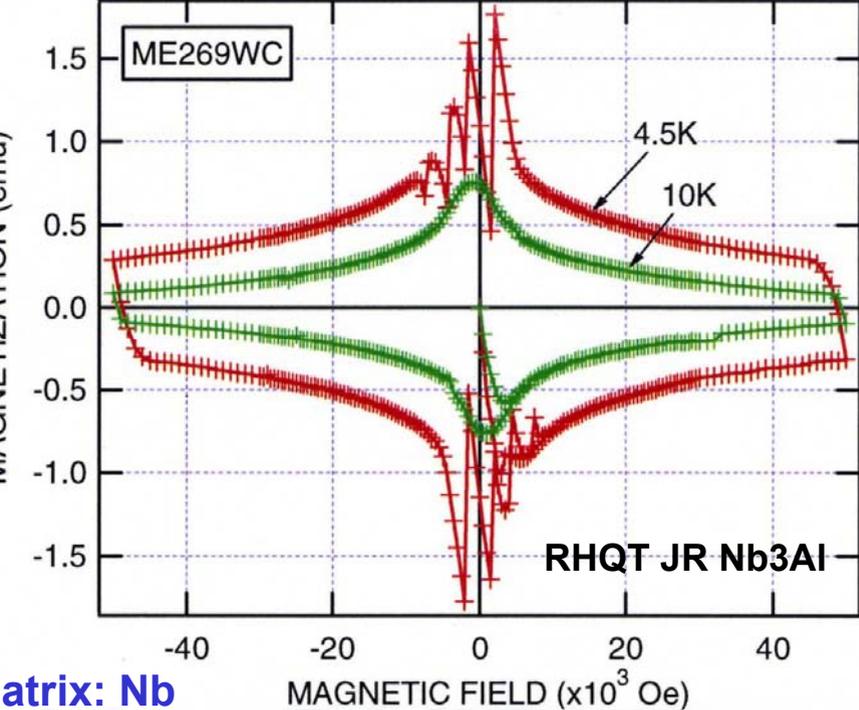


0.8 mm  $\Phi$

# Measurement\_1

V taps spacing: 100 mm, 375 mm  
Current ramp rate: 30A/sec, 60A/sec



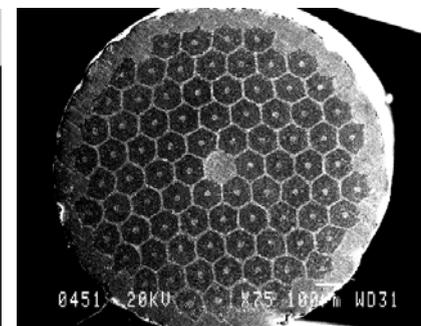
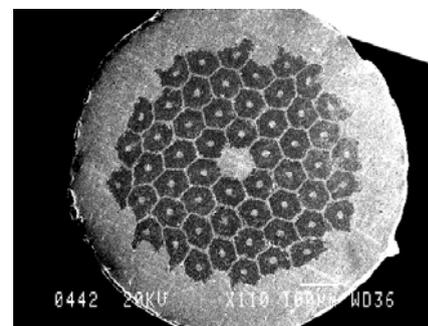
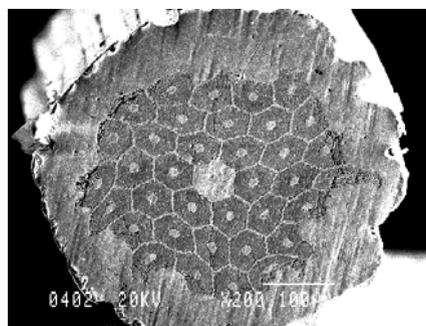


**Table 1** Specifications of measured JR Nb<sub>3</sub>Al wires.

Sample	#1	#2	#3
Diameter of wire (mm)	0.507	0.89	1.275
Number of filaments	36	84	84
Diameter of filament ( $\mu\text{m}$ )	55	76	108
Average thickness between filaments ( $\mu\text{m}$ )	2.8	6	9.4
Nb/Non-Nb ratio	1.5	1.39	0.59

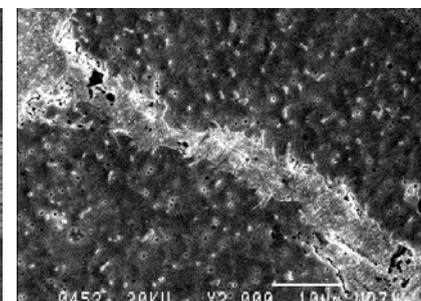
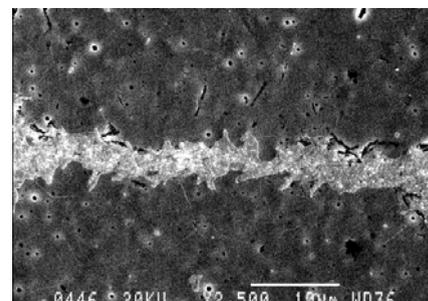
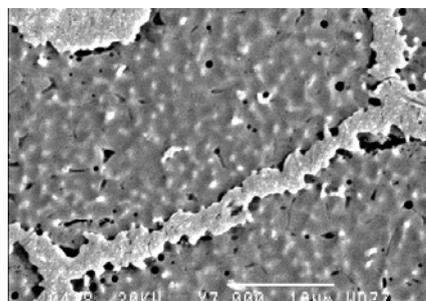
## Matrix: Nb flux jump

Not desirable for fusion  
and accelerator magnets



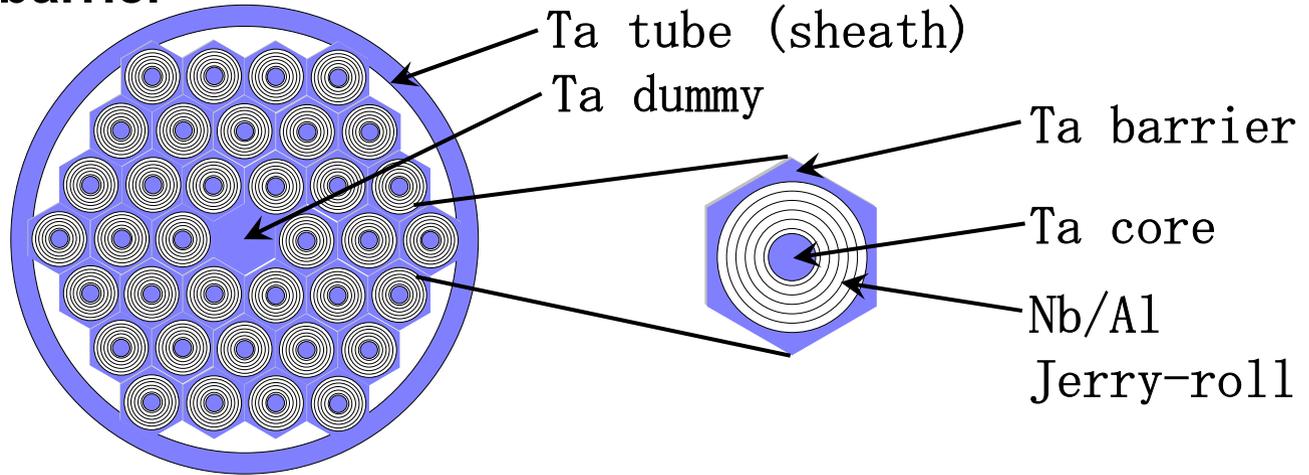
## AC Loss

- bridging
- proximity effect

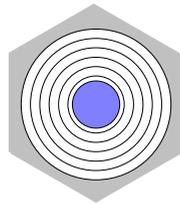


# Manufacture of Ta matrix JR Nb<sub>3</sub>Al wire

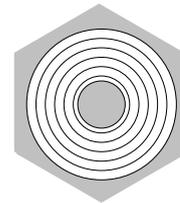
## Ta core-Ta barrier



## 2 other filament structures



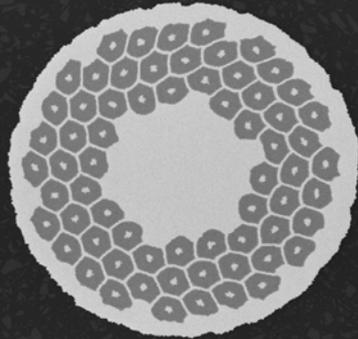
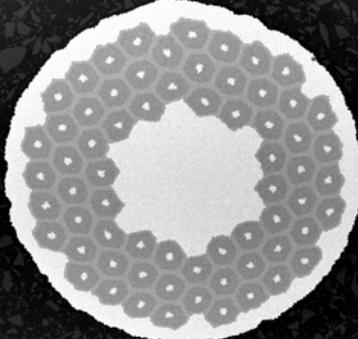
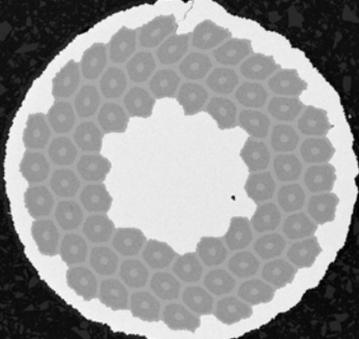
**Ta core-Nb barrier**



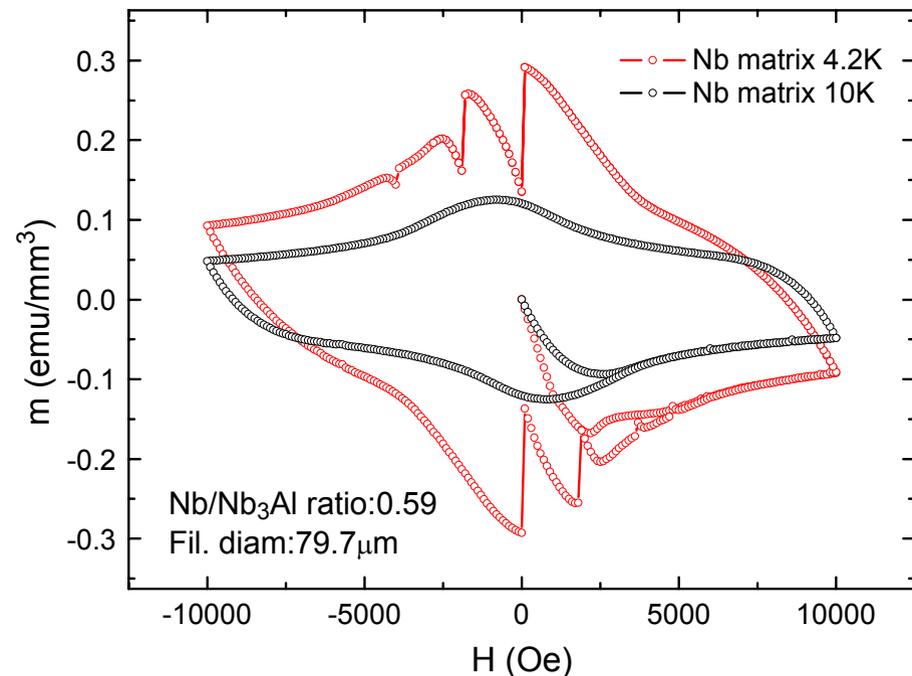
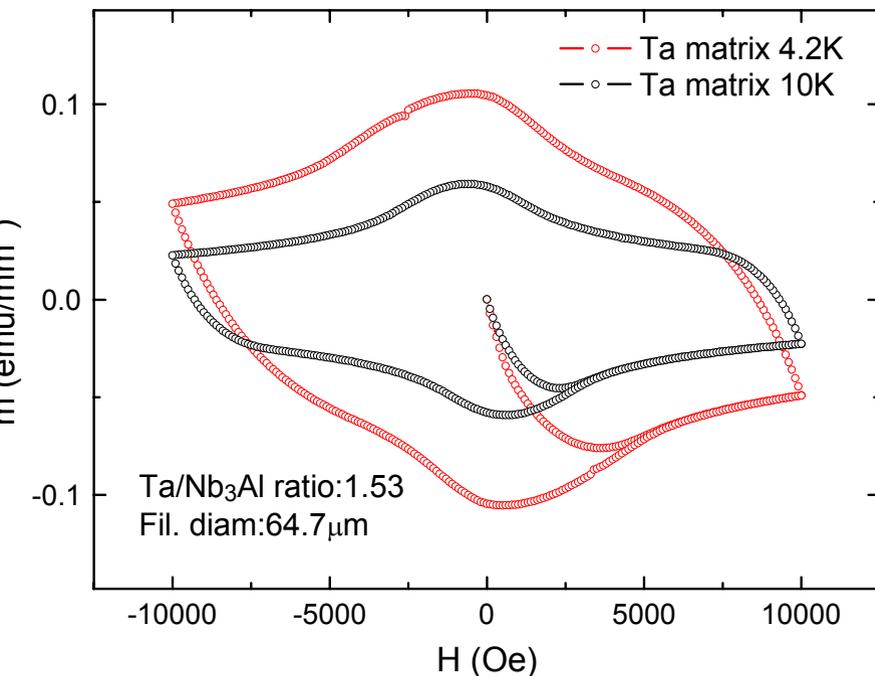
**Nb core-Nb barrier  
(conventional)**

# Workability

Wire Diameter	No of filaments	Filament diameter	Matrix ratio (non JR / JR)
Φ 0.8mm	66	φ 65 μ m	1.5

Structure	Ta core-Ta barrier (フィラメント間:Ta JRコア:Ta)	Ta core-Nb barrier (フィラメント間:Nb JRコア:Ta)	Nb core-Nb barrier (フィラメント間:Nb JRコア:Nb)
Cross section			
Workability	Very Good (no breakage until φ 0.5mm)	Good (no breakage)	Good (no breakage)

# Magnetization curve



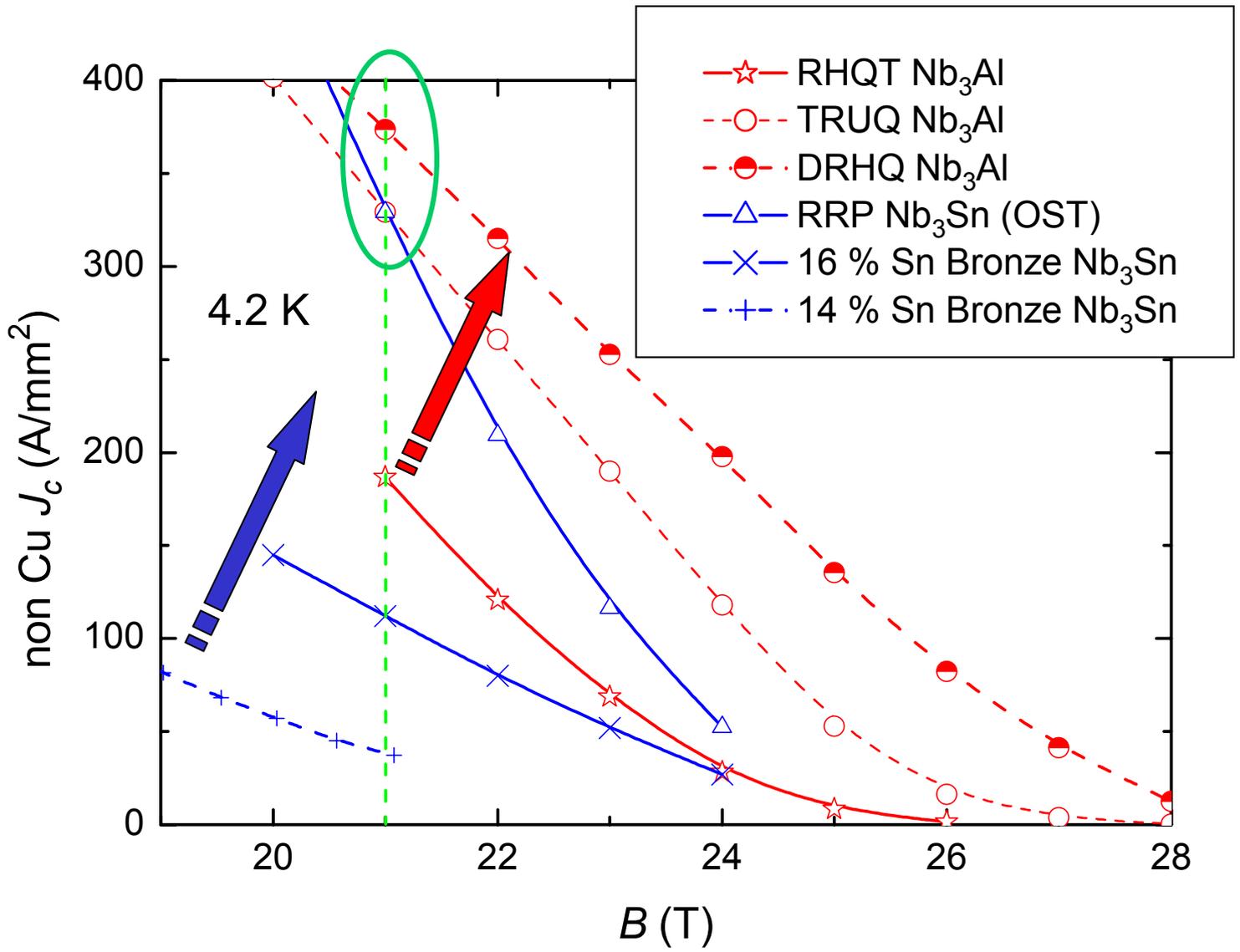
Ta matrix

→ suppression of flux jump

Other advantages

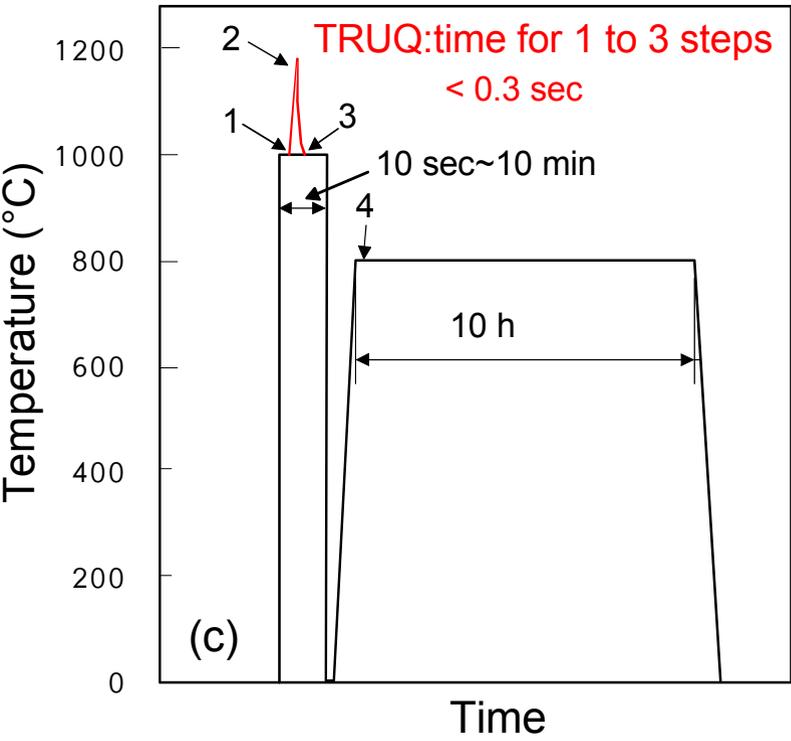
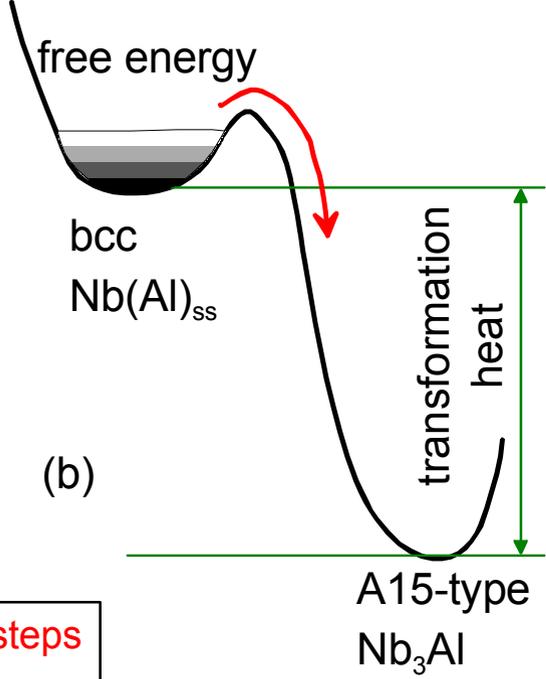
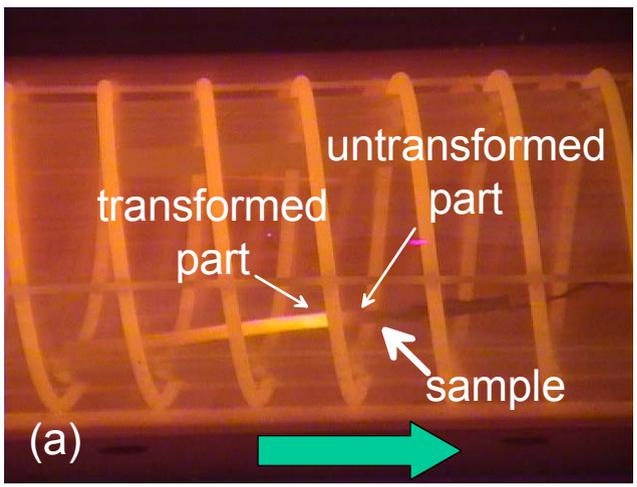
- high strength at high temperature
- no formation of Ga-rich compound on a surface
- less induced-radioactivity

# Potential of RHQT Nb<sub>3</sub>Al



# TRUQ

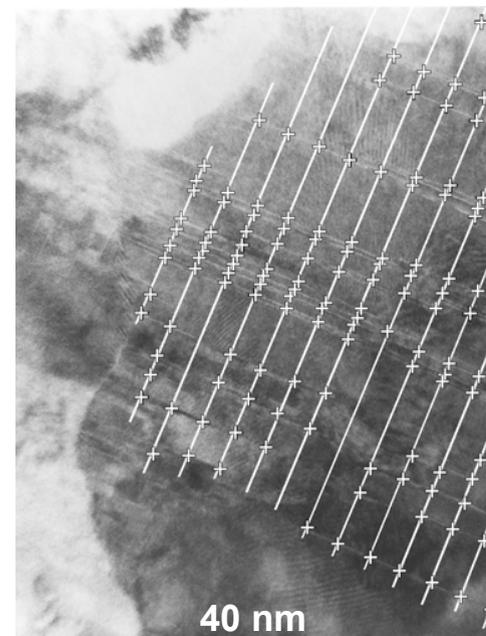
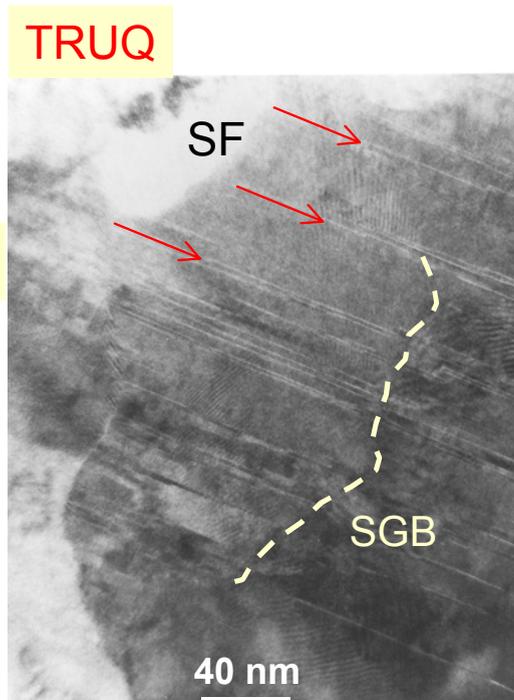
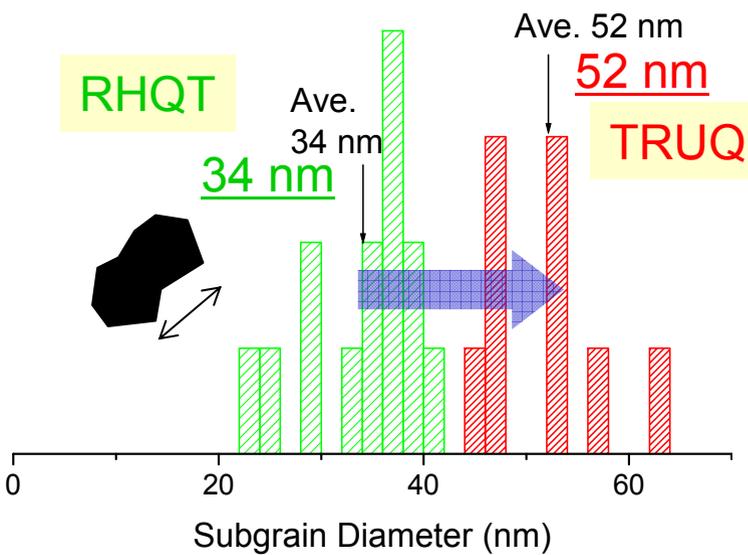
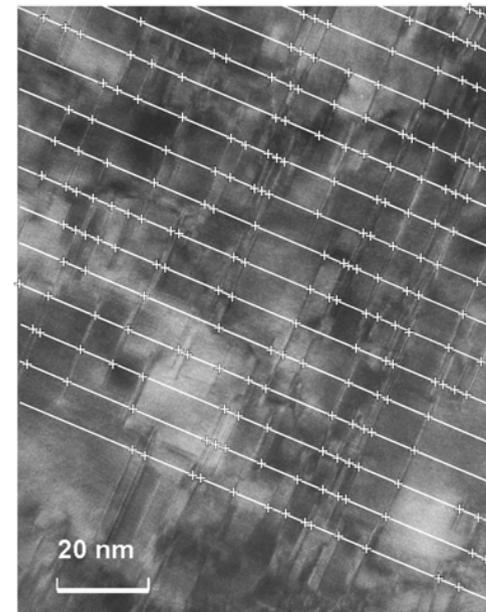
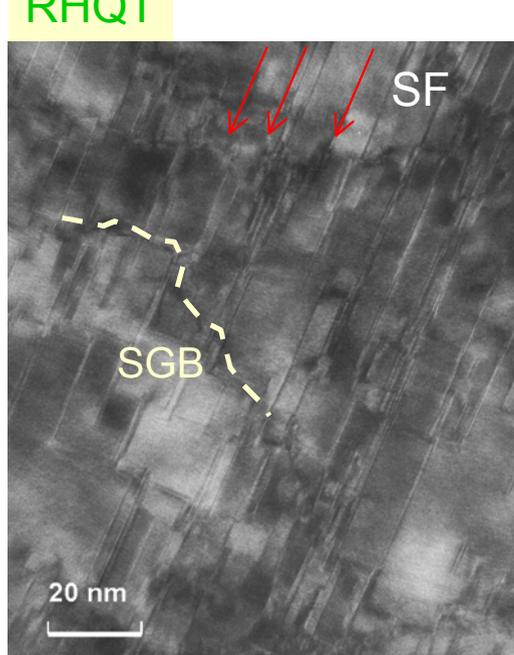
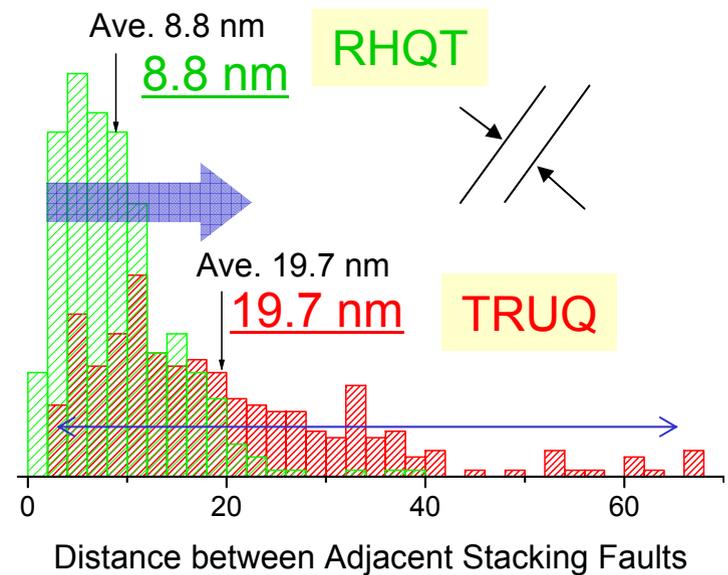
similar to a *combustion synthesis*

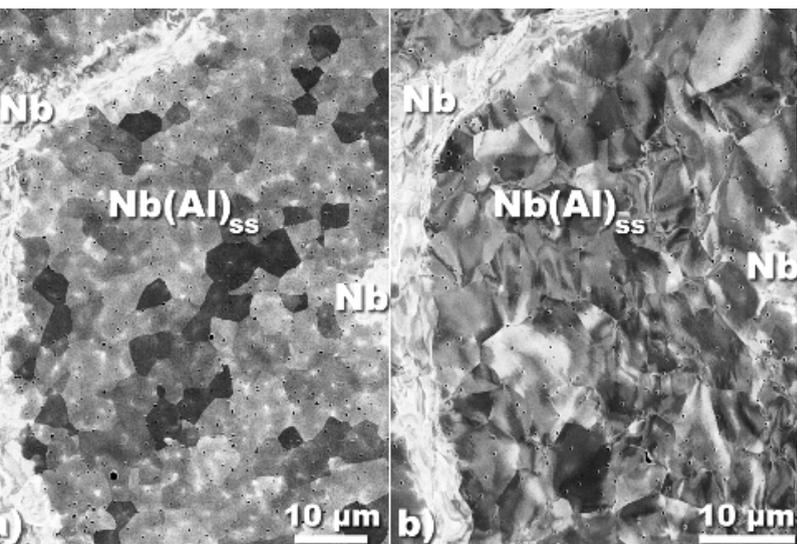


## TRUQ (*TR*ansformation-heat-based *Up-Q*uenching)

1. **ignition** (nucleation of transformation)
2. **thermal explosion**
  - **propagation** of the transformation interface
  - transform to A15 via **highly disordered bcc phase**
    - low long-range order
    - free from stacking faults**
3. **self-turn down** to ambient temperature
4. annealing for **long-range order**

# Microstructure





a) as-quenched wire at 1.27 mm and b) after Cu-cladding and forming into tape.

Microchemical homogeneity  
in filaments

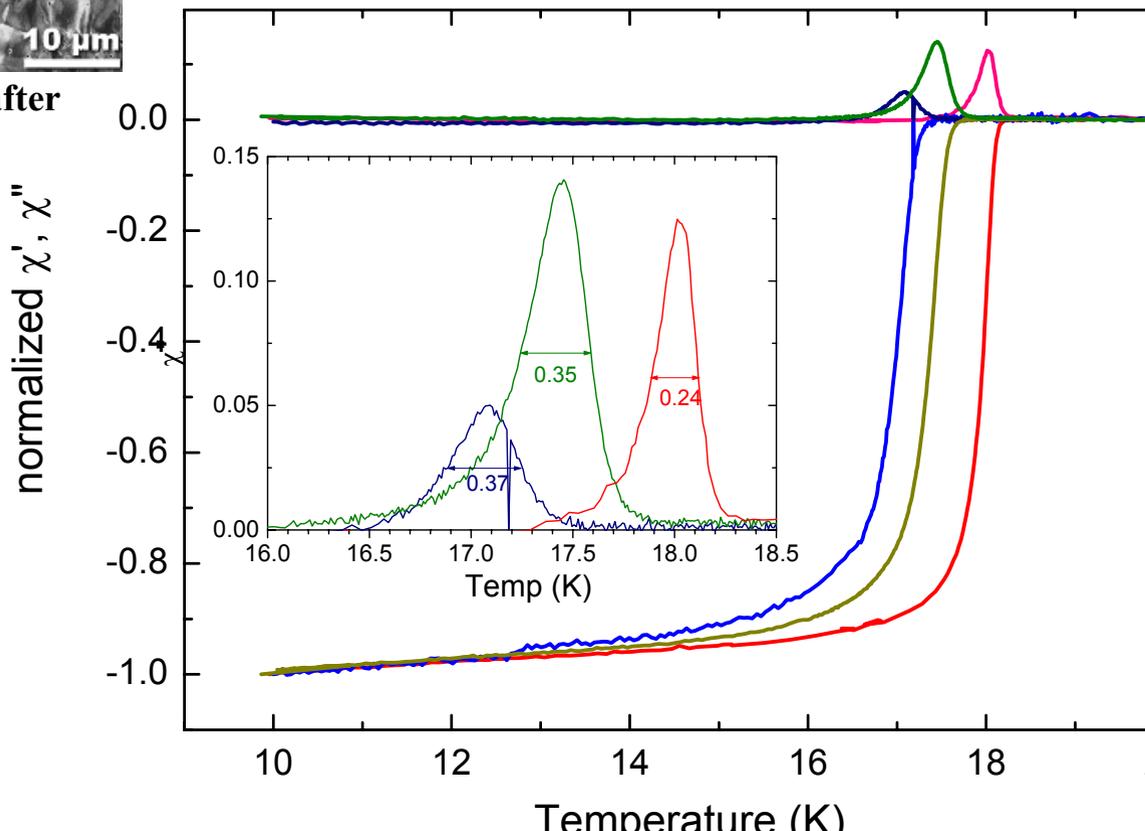
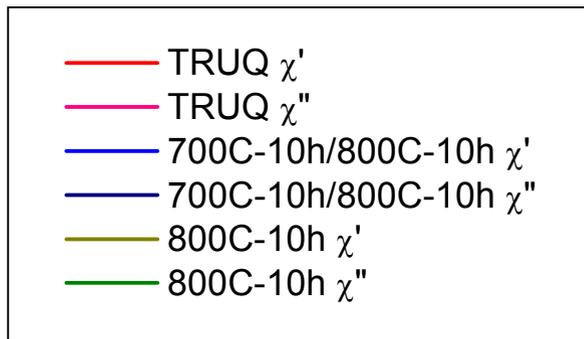


Sharp transition



Enhancement in  $J_c$

# Non-uniformity



# Optimization for $J_c$

under the condition of **ordinary transformation**  
that enables W&R coil ( $\sim 800^\circ\text{C}$ , ramp rate of 1-5 h/ $800^\circ\text{C}$ )

## Parameters

- Wire diameter
- **Nb matrix ratio**
- No. of JR filaments
- Filament diameter
- **Inter-filament spacing**
- Nb/Al ratio
- layer thickness
- Alloying
- Joule heating current density
- Heating distance
- Wire speed at RHQ
- **R.A. after RHQ**
- **Transformation HT**

**Microchemistry**

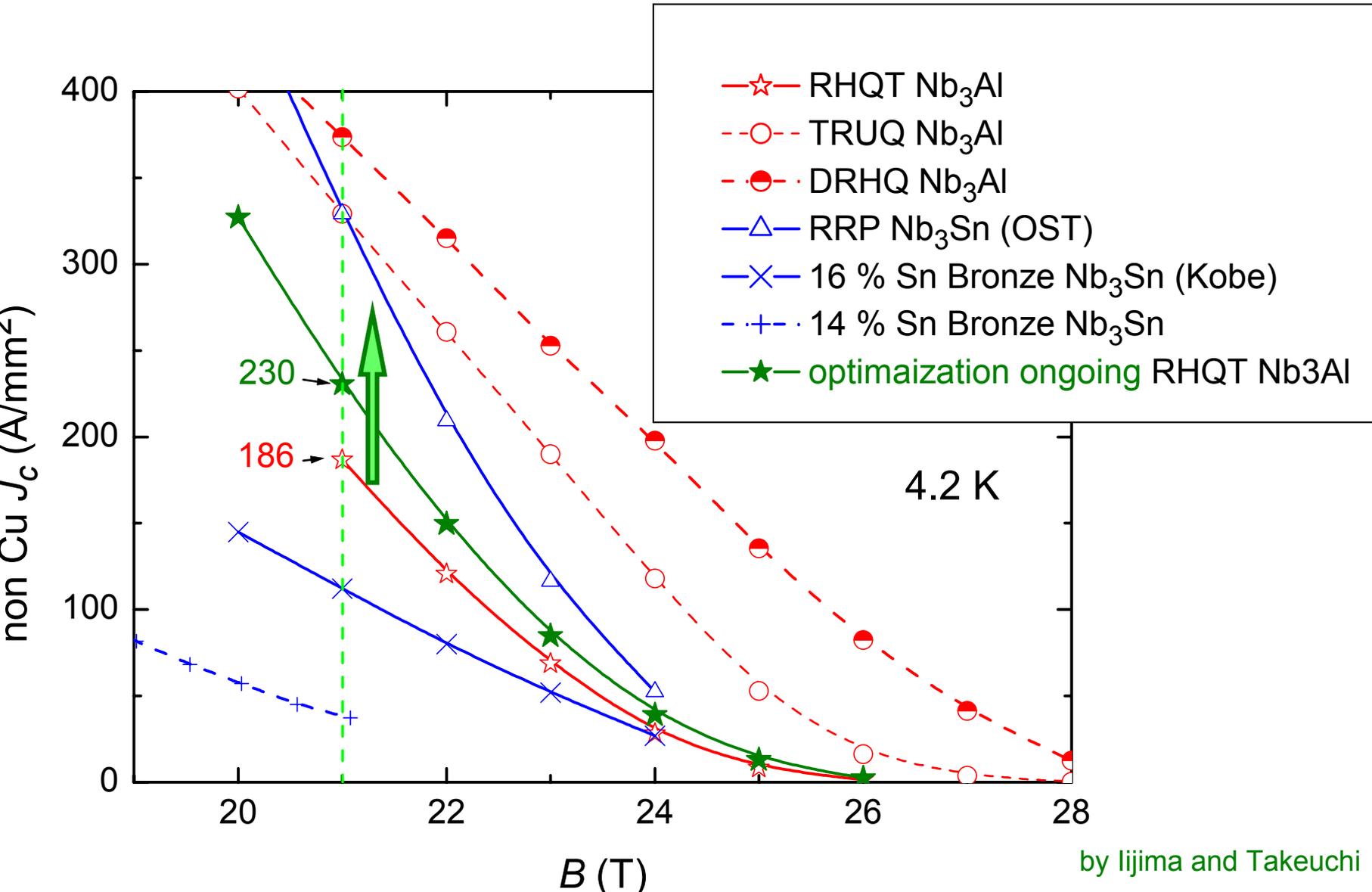
**Crystal imperfection**

bcc grain, ordering

A15 grain

Stacking faults

# Ongoing improvement of JR Nb<sub>3</sub>Al



# Development Schedule

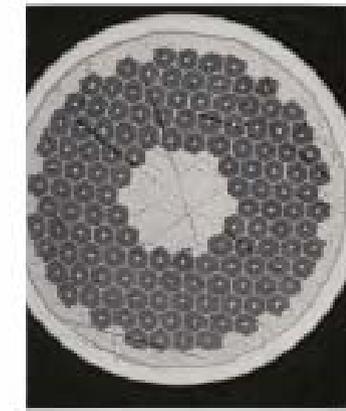
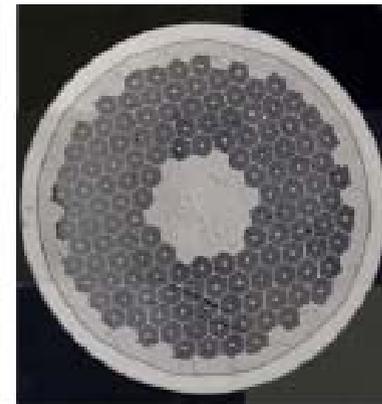
- Long-length of precursor ( $>2\text{km}$ )  
large billet
- Long-length of RHQ processing ( $>2\text{km}$ )  
large-scale RHQ apparatus: under construction
- Reel-to-reel Cu ion plating  
installation, trial operation

Target: piece length of more than 2 km for 1.35 mm $\phi$  wire

# Multifilament billet (50kg)

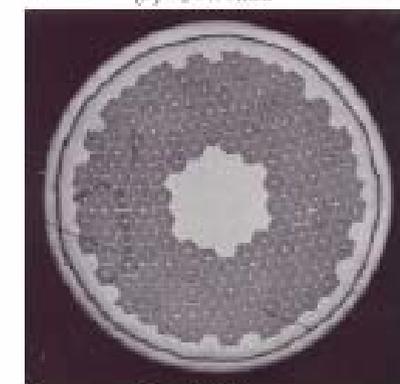
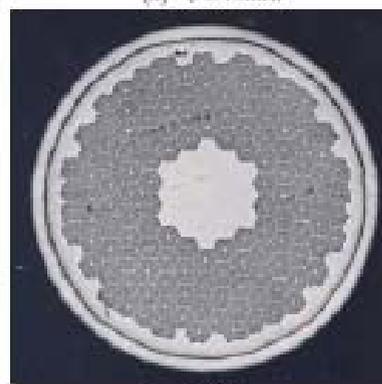
Φ 8.4 mm

Φ 5.9 mm



(a) Φ 8.40mm

(b) Φ 5.90mm



Φ 2.9 mm

(c) Φ 2.90mm

(d) Φ 1.75mm

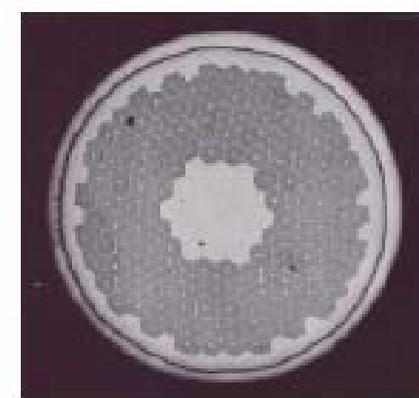
Φ 1.75 mm

No breaking during drawing of wire



piece-length: 2.6 km for Φ 1.35 mm wire

(corresponding to 9.7 km for Φ 0.7 mm wire)

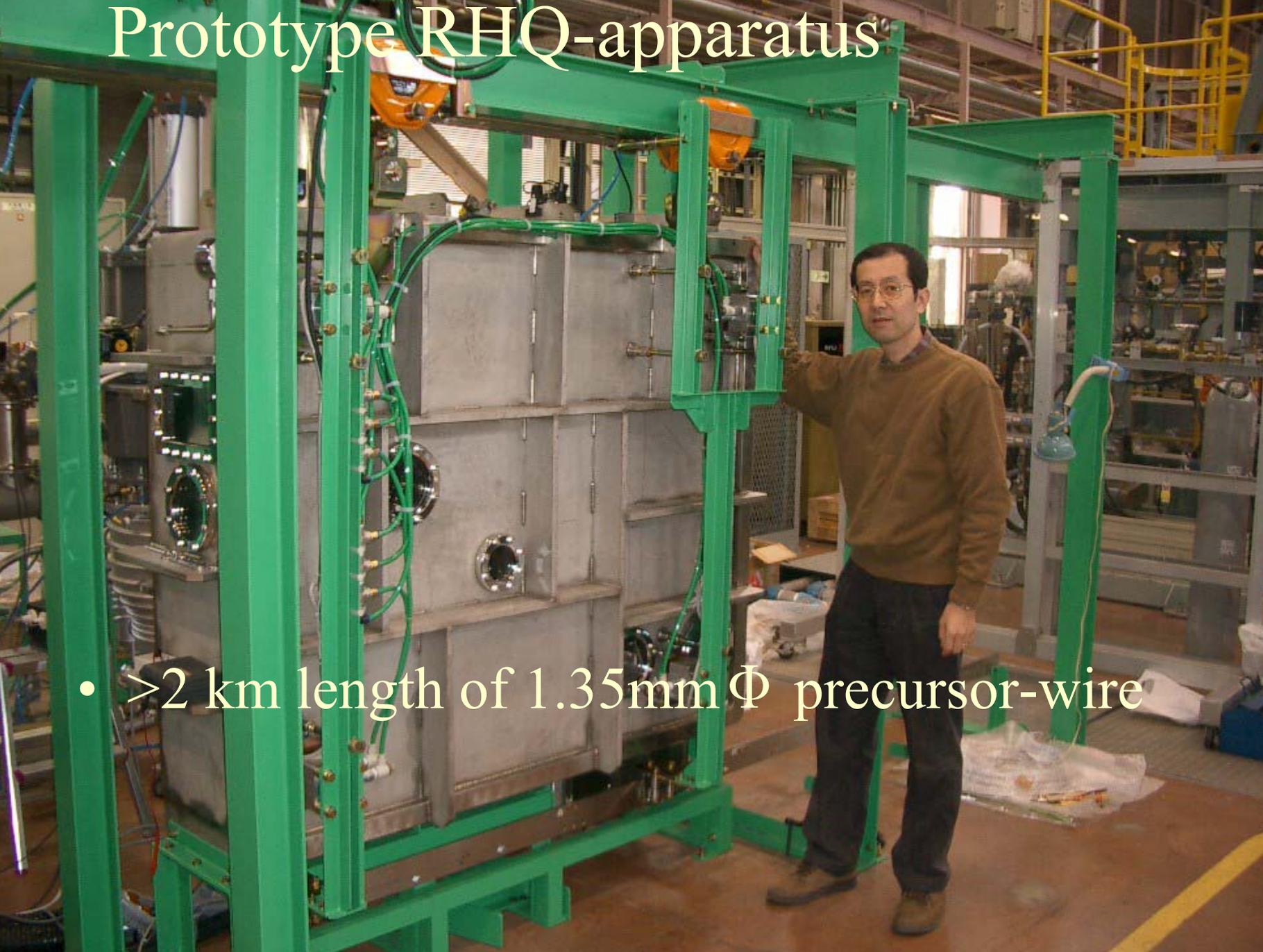


(e) Φ 1.50mm(最終線徑)

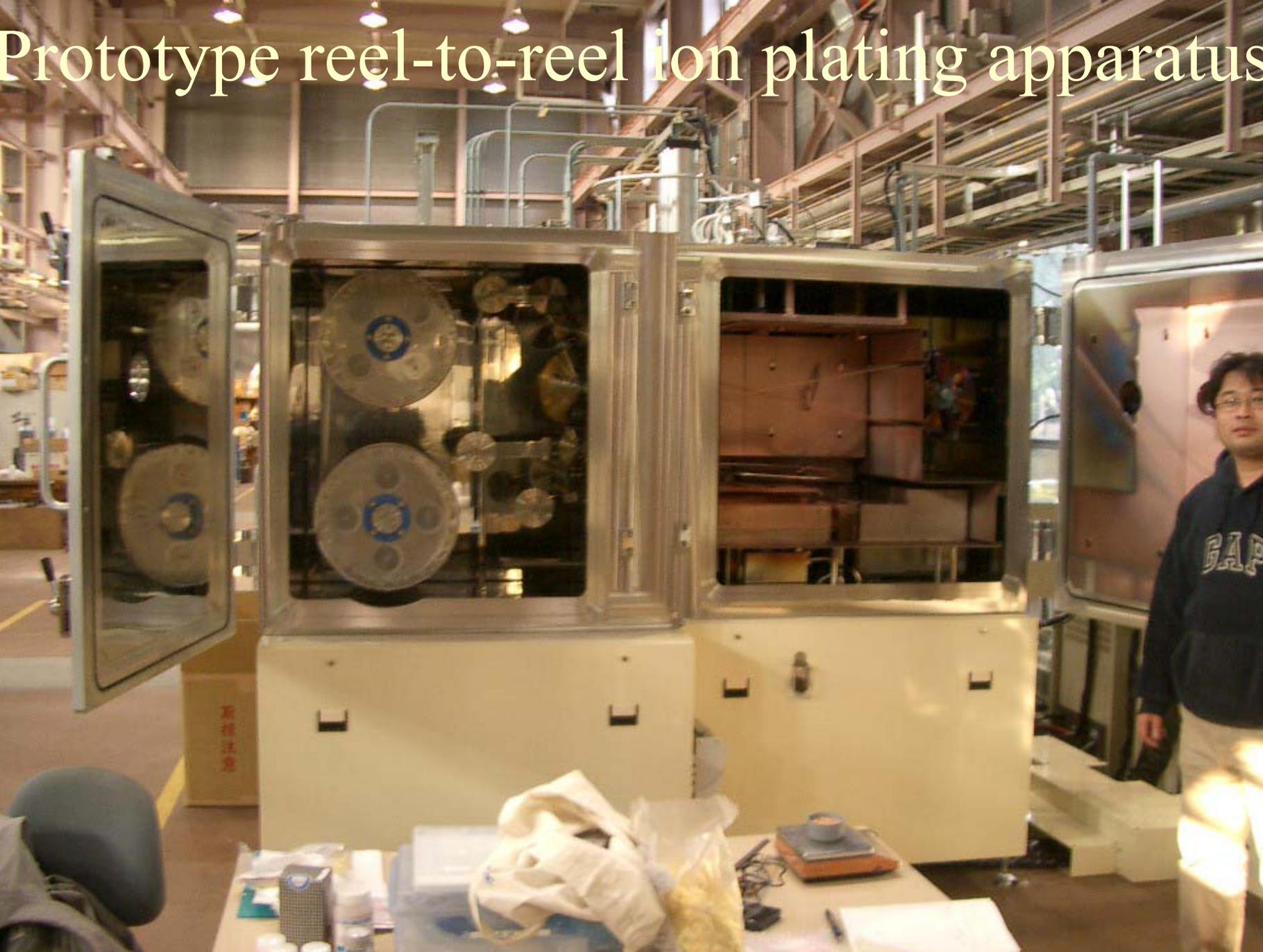
Φ 1.50 mm

# Prototype RHQ-apparatus

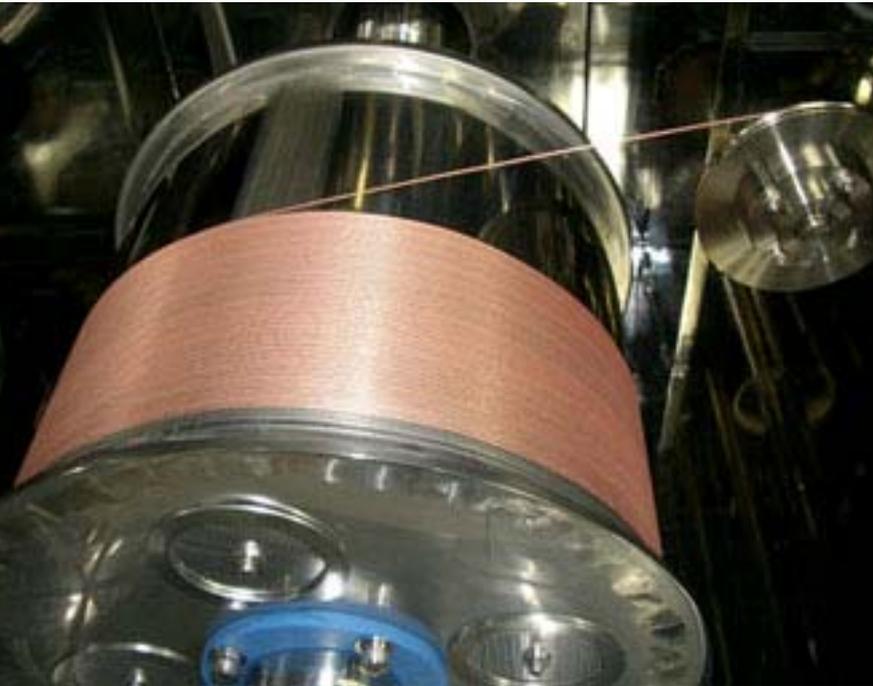
- $>2$  km length of  $1.35\text{mm } \Phi$  precursor-wire



# Prototype reel-to-reel ion plating apparatus



# Reel-to-reel Cu ion plating apparatus\_2



# Summary

- Large multifilament billet: 52 kg
- Piece length of precursor (1.35 mm): 2.6 km
- RHQ apparatus: just installed  
300 m → ? km
- Non-Cu  $J_c$  improvement (21T): Ongoing
- Stabilization of a round wire  
internal stabilization  
Cu ion plating and electroplating